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Active Truss for Fast Response Tip Clearance Modulation

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NASA Aeronautics Research Mission Directorate (ARMD)

FY12 LEARN Phase I Technical Seminar

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Outlines

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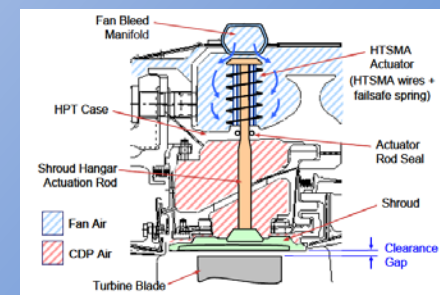
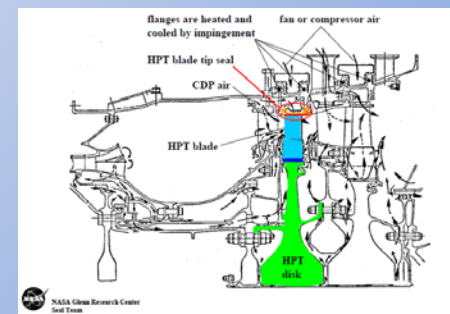
- The innovation
- Technical approach
- Impact of the innovation
- LEARN Phase I Results
- Summary
- Next steps



Need for Innovation

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- Current State of Technology
 - Thermal expansion and contraction of entire shroud/case (Active Case Cooling)
 - Slow response and scheduled modulation
 - huge thermal mass with seal segments directly mounted on engine casing,
 - ineffective heating or cooling of the shroud via convection between shroud surfaces and air.
 - No asymmetry modulation
- Prior Research
 - Mechanical/Smart materials/Hydraulic/Pneumatic
 - External to engine case/shrouds and moving parts
 - Incompatibility with environment for HPT
- Need for Innovation
 - Fast Response Tip Clearance Modulation Mechanism
 - Light weight, compact and environmental compatible to HPT
 - Integral to shroud-case structure w/o moving parts



DeCastro, etc, 2005



Impact of Innovation

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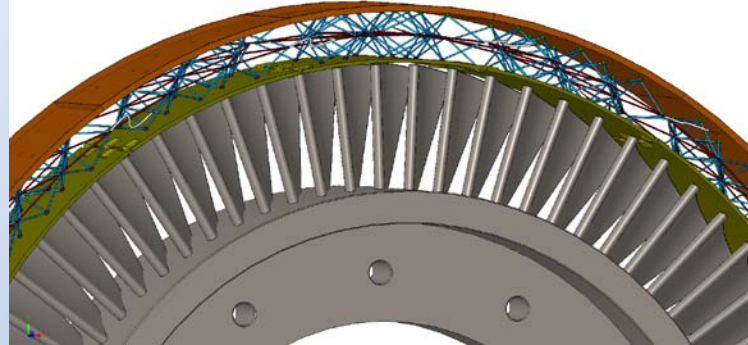
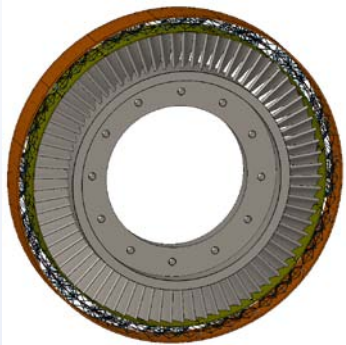
A Fast Response Tip Clearance Modulation

- Enable turbine tip clearance set to “optimal” during longest flight segment (cruise)
- Reduce specific fuel burn (SFC) and exhaust gas temperature (EGT)
 - 0.01” in turbine blade tip clearance equals:
 - 1 % in SFC
 - 10° C in EGT
- Low CO₂ emission
- More time on wing



Innovation-Active Truss Modulation

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Approach:

- Variable geometry active truss for tip clearance modulation
- Truss actuation by thermally induced strains
- Low thermal mass and large surface area for heat exchange

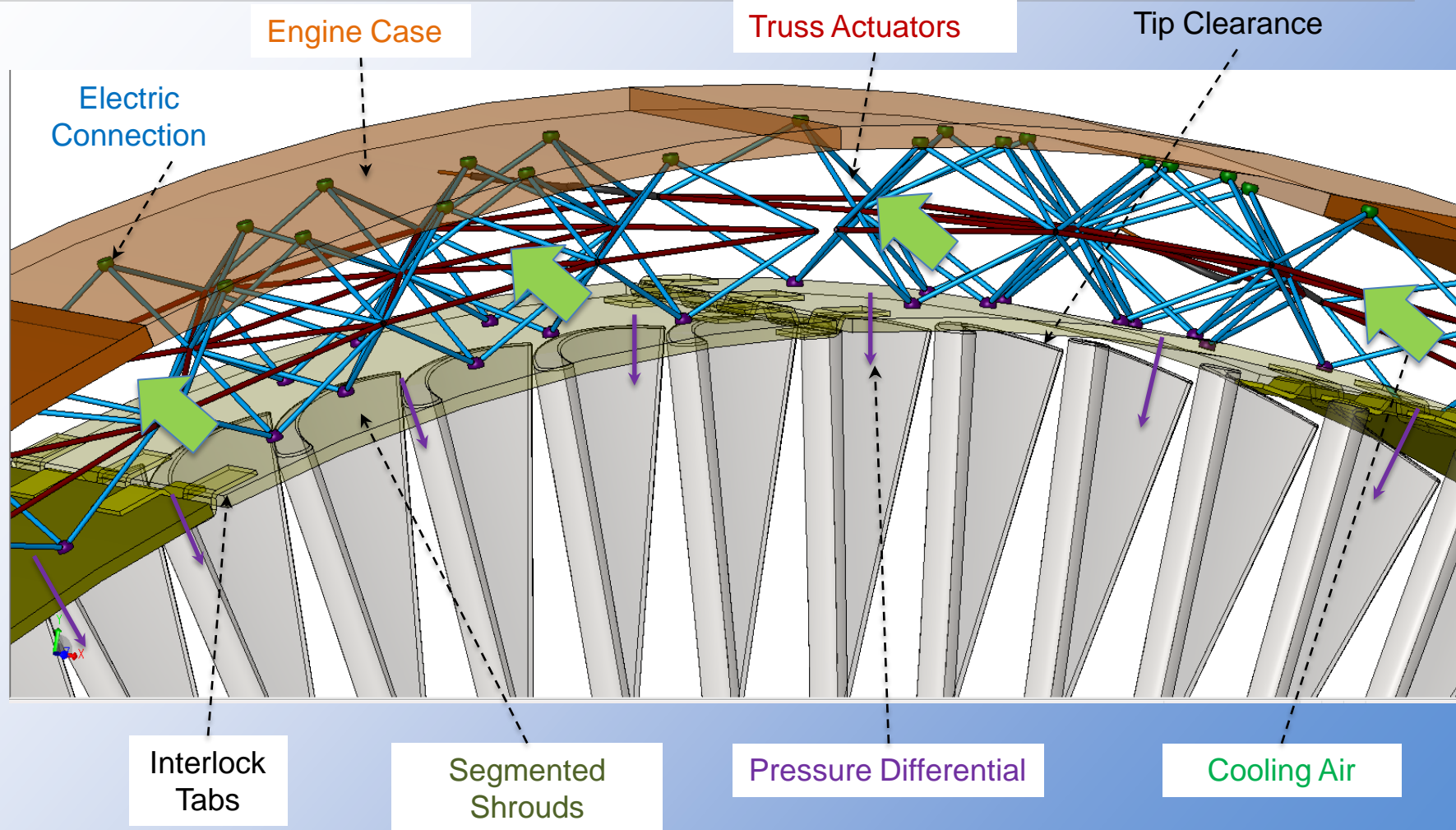
Benefits:

- Sustain benefits of thermal expansion approach
- Fast Response-one order of magnitude improvement
- Light weight and Integral to shroud-case structure
- Asymmetric and symmetry clearance modulation



Active Truss Modulation (ATM)

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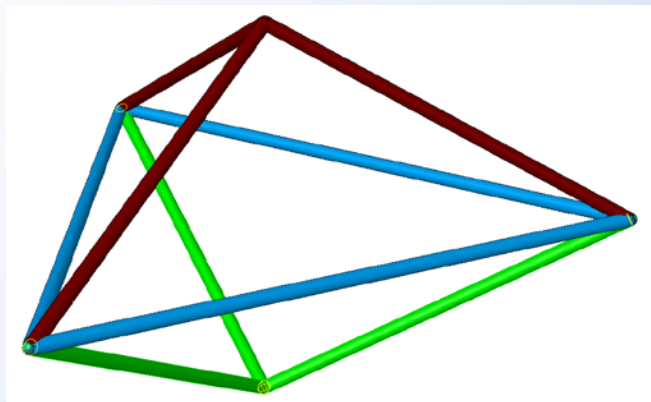




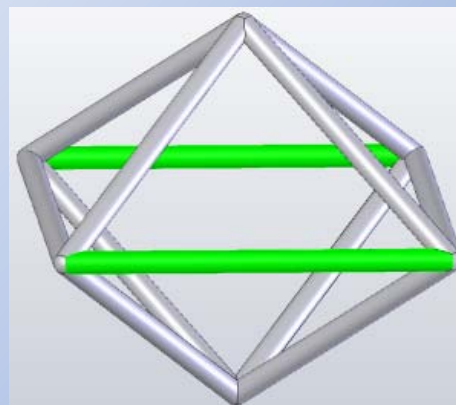
Core Elements of Truss Actuation

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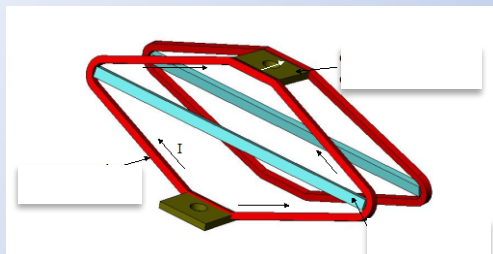
Prime Movers



Dual Tetrahedron



Dual Pyramid



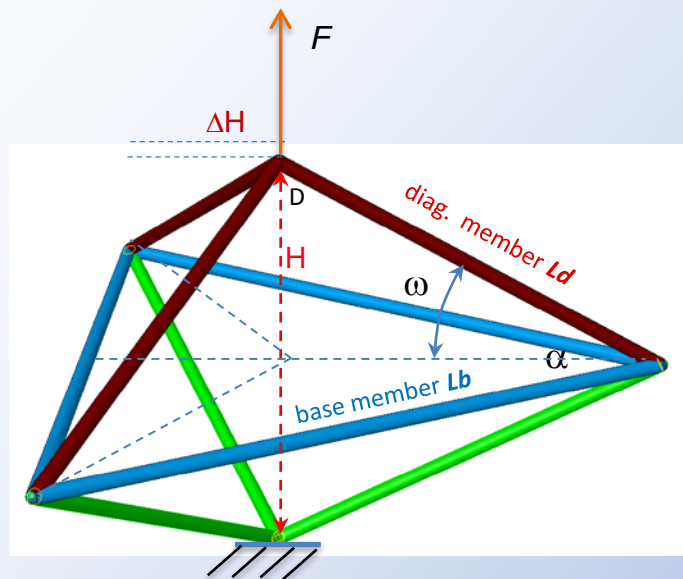
Parallel *Theta* Ring (2D)

- Actuation by linear thermal expansion
- Structural amplification of displacement
- Multiple inputs and single output actuation
- Low thermal mass and volume density (<0.1)
- One order of magnitude faster response than engine case cooling (ACC)



Principle of Truss Actuation

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For thermally induced actuation

- Displacement
- Stiffness
- Response
- Temperature

$$H = 2\sqrt{l_d^2 - \frac{l_b^2}{3}} = 2l_d \sqrt{1 - \cos^2 \omega}$$

Actuation displacement

$$\frac{\partial H}{\partial l_d} = \frac{2l_d}{\sqrt{l_d^2 - l_b^2 / 3}} = \frac{2}{\sqrt{1 - \cos^2(\omega)}}$$

$$\frac{\partial H}{\partial l_b} = \frac{-\frac{2}{3}l_b}{\sqrt{l_d^2 - l_b^2 / 3}} = \frac{-\frac{2\sqrt{3}}{3}\cos(\omega)}{\sqrt{1 - \cos^2(\omega)}}$$

Tip clearance modulation

$$\Delta H_t = \sum_{j=1 \sim 6} \frac{\partial H}{\partial l_d^j} dl_d^j - \sum_{i=7 \sim 9} \frac{\partial H}{\partial l_b^i} dl_b^i$$

Thermal expansion in each members

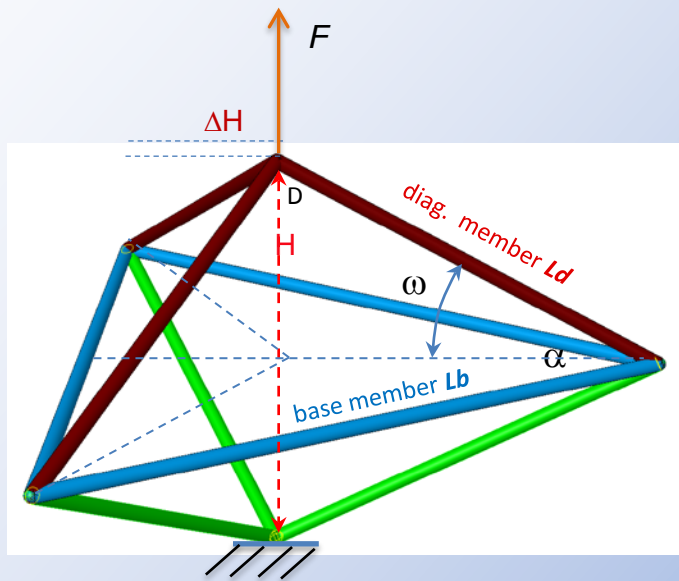
$$dl_d = l_d^j C_{ted} \Delta T_{l_d}$$

$$dl_b = l_b^i C_{teb} \Delta T_{l_b}$$



Principle of Truss Actuation

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Structural stiffness

$$K_D = \frac{9k_d k_b \sin^2 \omega}{4k_d \cos^2 \omega + 6k_b}$$

Total displacement modulation

$$\Delta H = \Delta H_t + F / K_D$$

Member buckling (L/r slenderness)

$$\sigma_{cr} = \frac{4\pi^2 E}{(L_b / d)^2}$$

Volume density (weight)

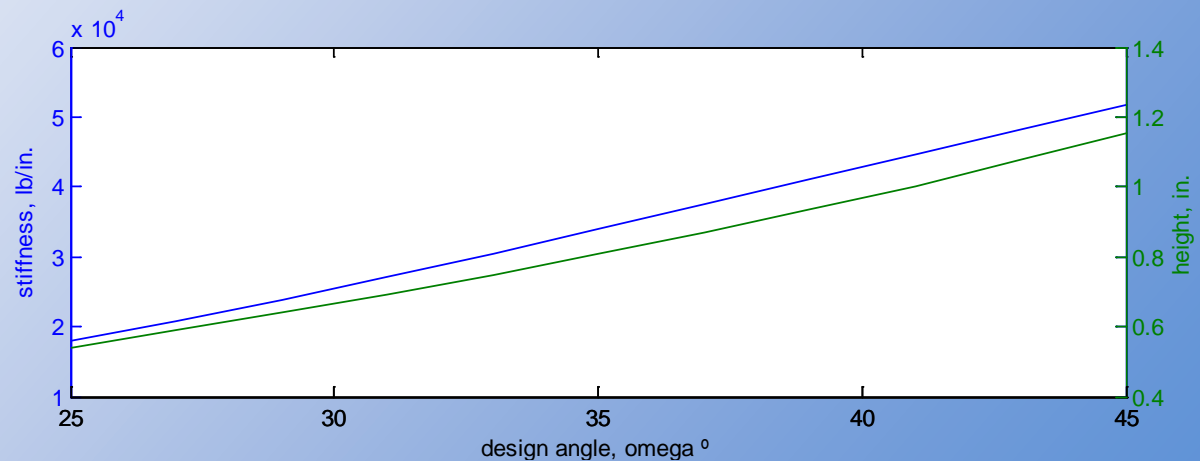
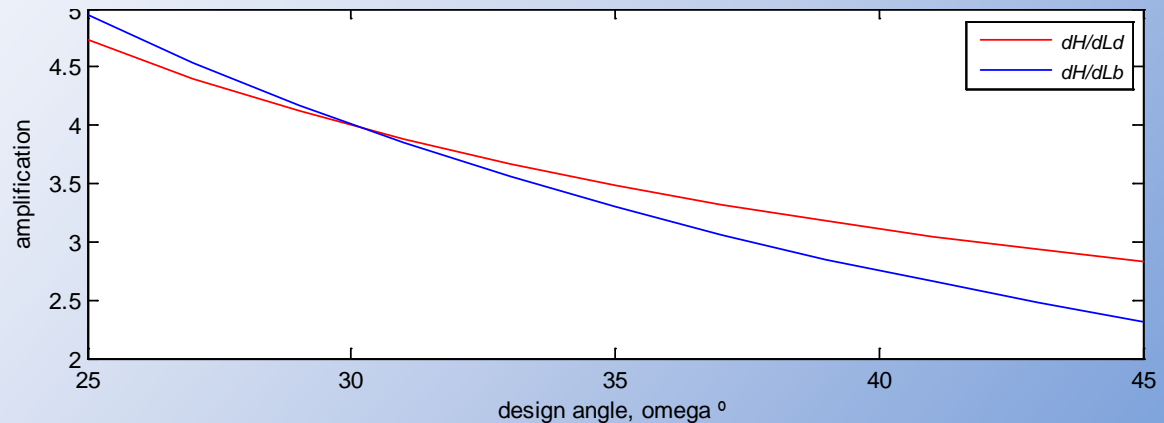
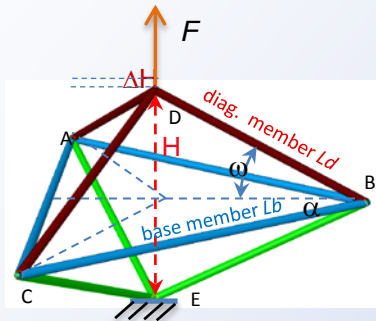
$$\bar{\rho} = \frac{\pi(3+2\sqrt{3}/\cos^2 \omega)}{\tan(\omega)} (d/l_b)^2$$



Design of Tetrahedron Truss

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Kinematic and Structural Design Envelope

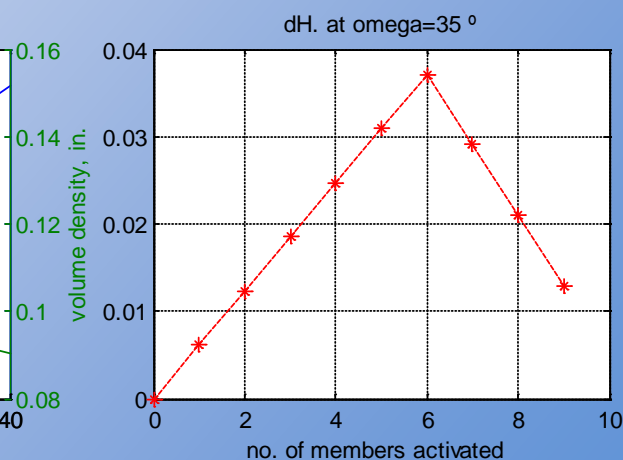
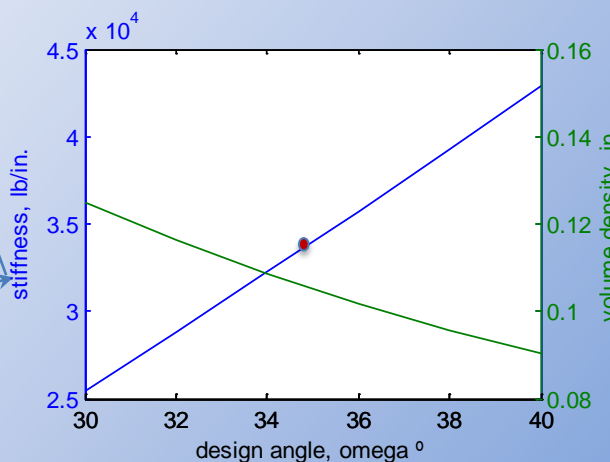
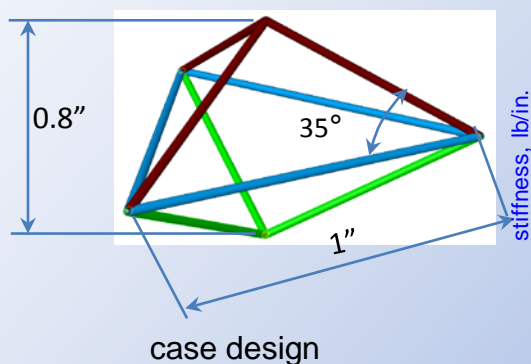
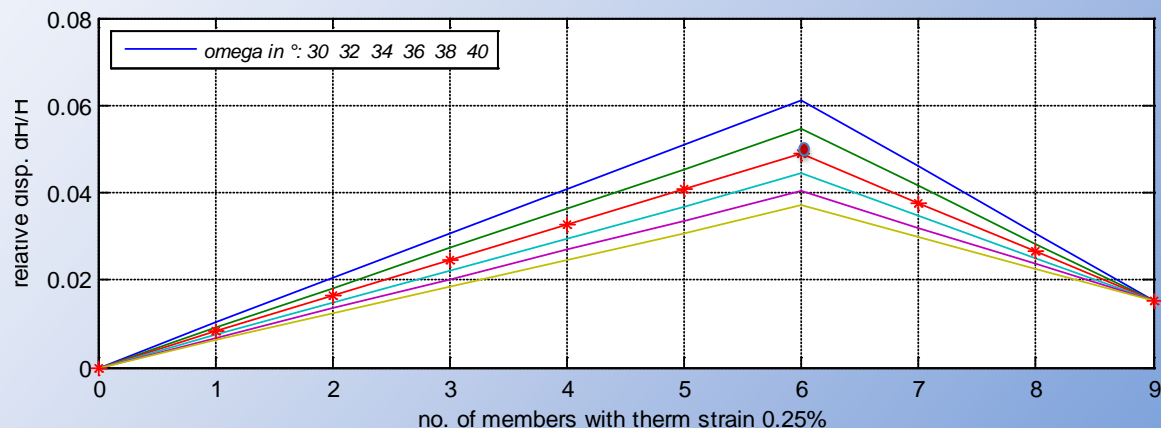
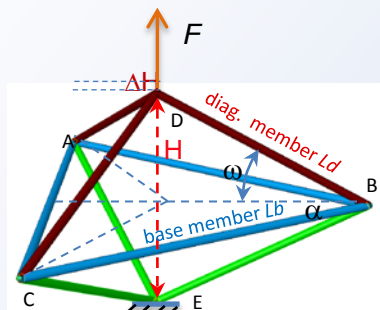




Design of Tetrahedron Truss

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Kinematic and Structural Design Envelope

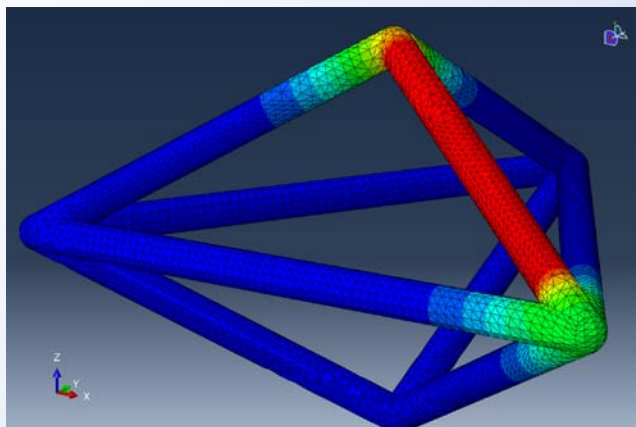




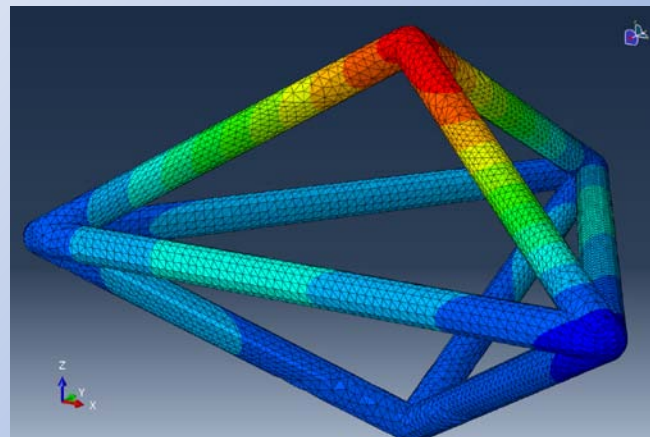
Design of Tetrahedron Truss

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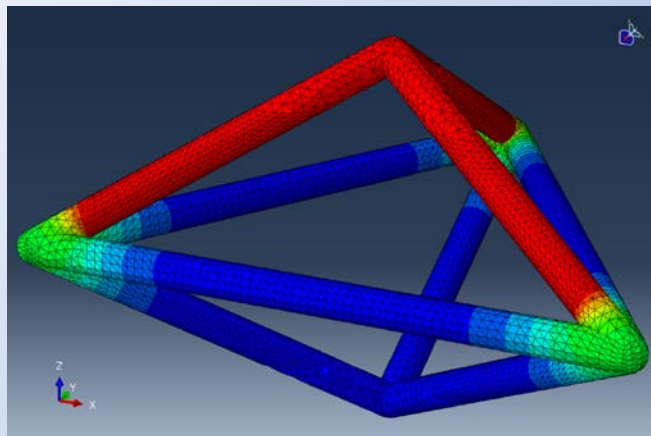
FEM Model



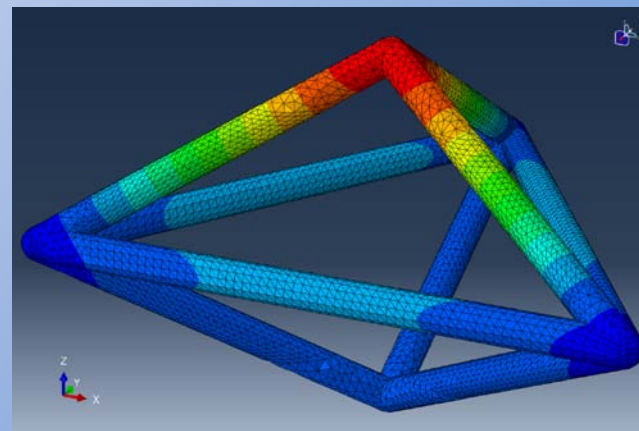
$\Delta T = 300^\circ\text{F}$ applied to 1 diag. member



Thermal expansion field



$\Delta T = 300^\circ\text{F}$ applied to 3 diag. members



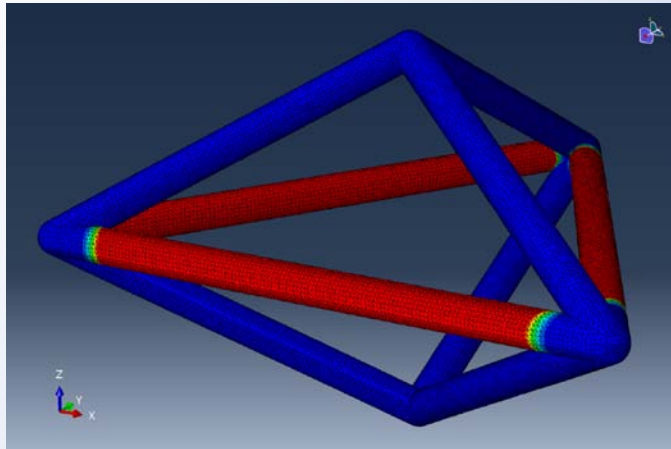
Thermal expansion field



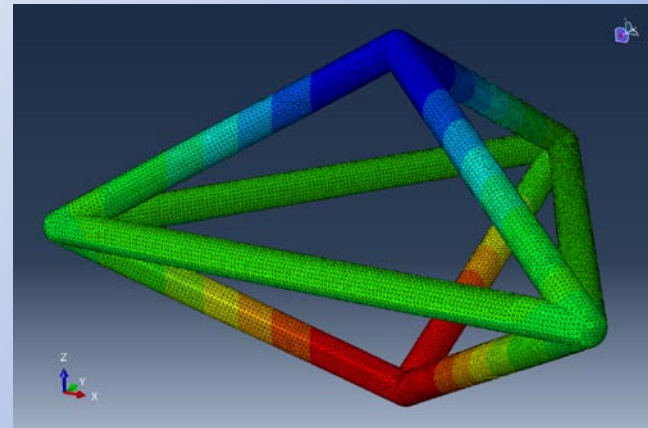
Design of Tetrahedron Truss

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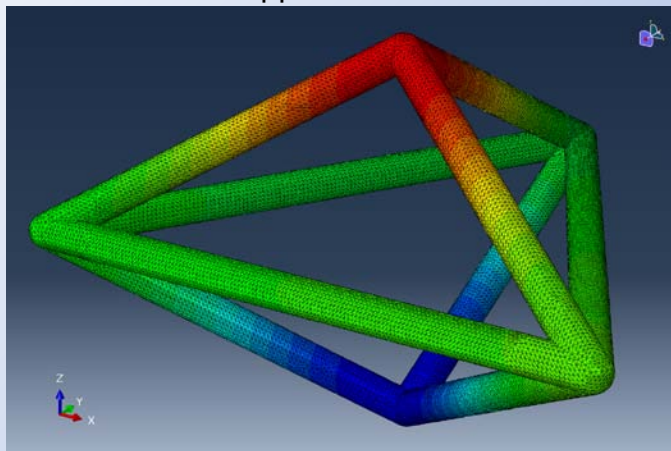
FEM Model (cont'd)



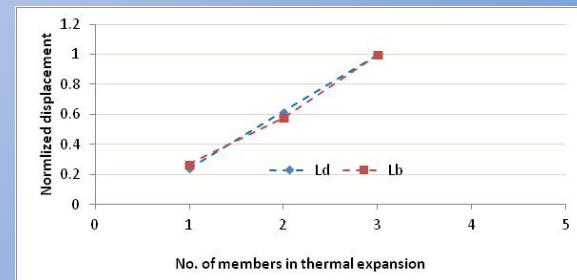
$\Delta T = 300^\circ\text{F}$ applied to 3 horizontal members



Thermal Expansion



Deformation field under load

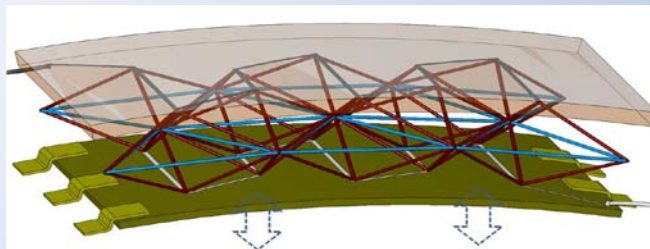
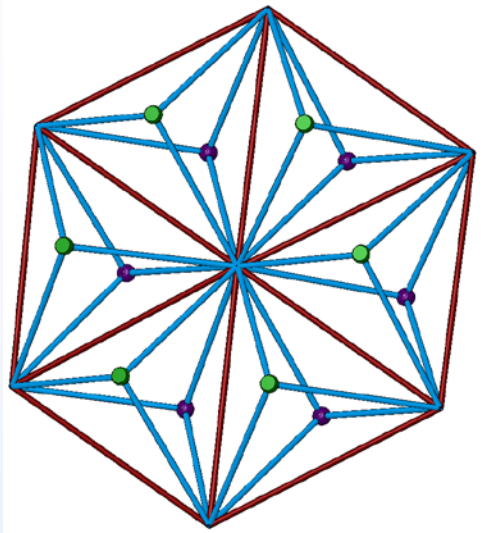


- Linear summation of thermal expansion by each member
- Max principal stress $\sigma_{\max} \ll \sigma_{\text{yield}}$ & σ_{cr} under $\Delta P = 180$ psi



Electric Activation of Truss Matrix

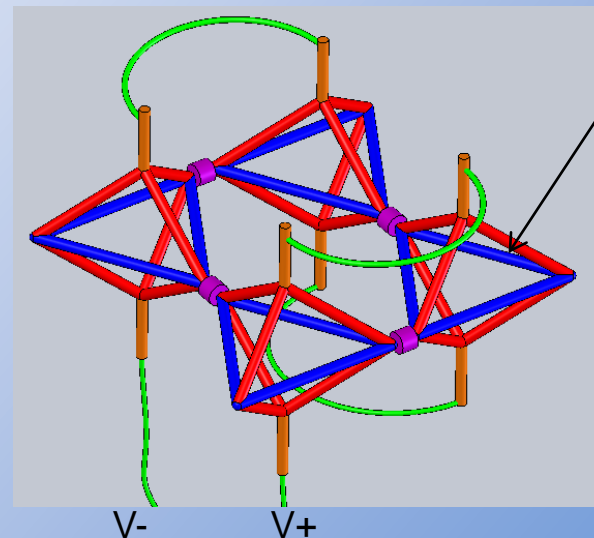
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Direct resistive heating topologies

- Heating each member individually
- Group collective heating (base and diagonal)
- Combination of series and parallel heating
- Intelligent heating-Wheatstone bridge effect

Challenge: Large current and low voltage



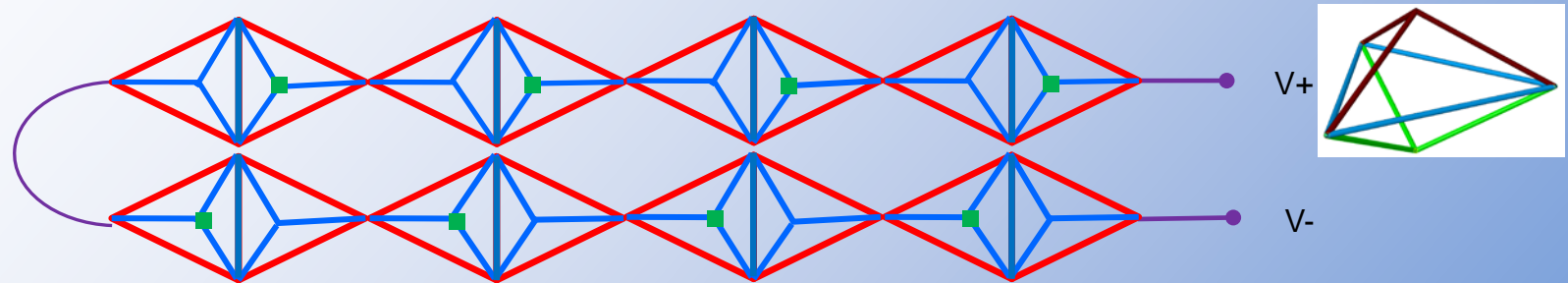
- Cell to cell series connection
- Full actuation
- Fail safe
- Embedded wiring in case



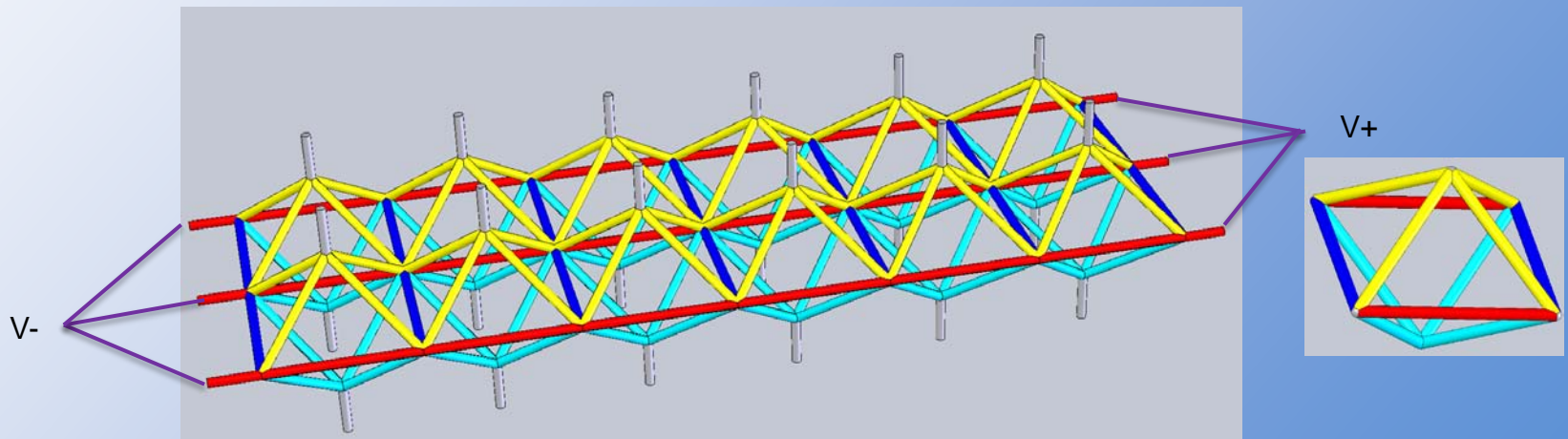
Electric Activation of Truss Matrix

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Series connection and partial grouping (2/3 activation)



Parallel/series connection and partial grouping (1/2 activation)



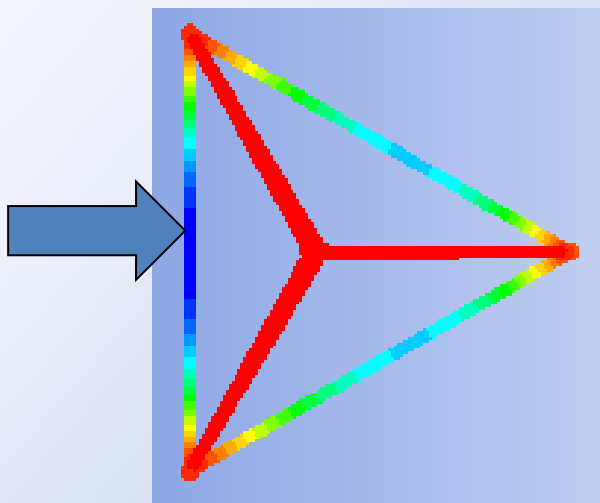
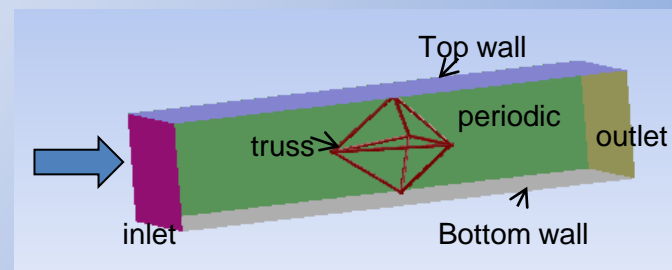


Air Cooling- Activation and Deactivation

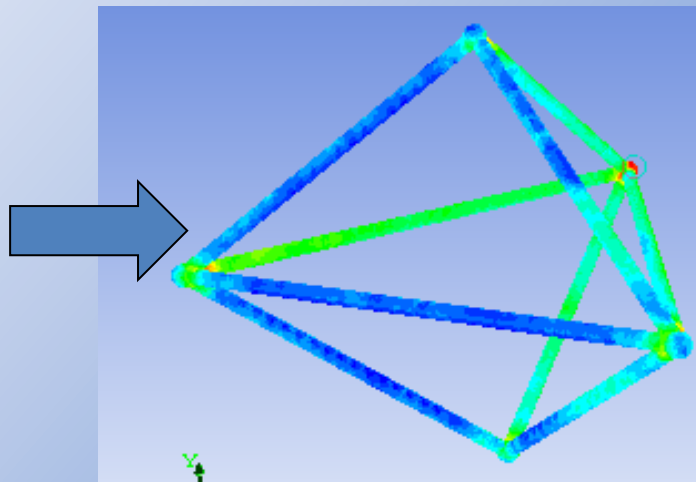
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Air Cooling Modeling

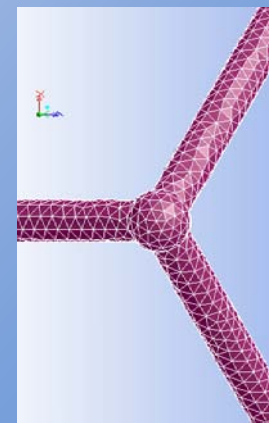
- Steady state heating/cooling
- Transient cooling



Remain activated,
electric power on



Deactivated, electric
power off

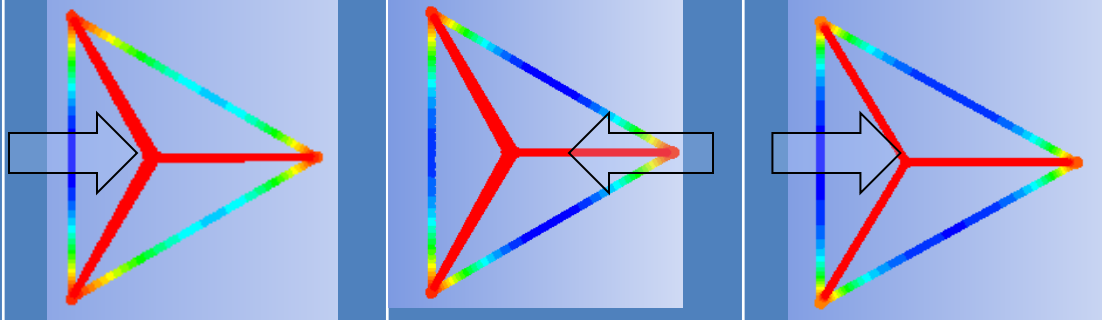




Air Cooling- Activation Mode

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To maintain temperature difference while electrically heated

Member temperature contours				
	Air flow (m/s)	0.1	0.1	10
	Temperature difference between heated and unheated wires (°C)	100	110	180
	Heat dissipation rate (W)	7.04	6.9	42.2

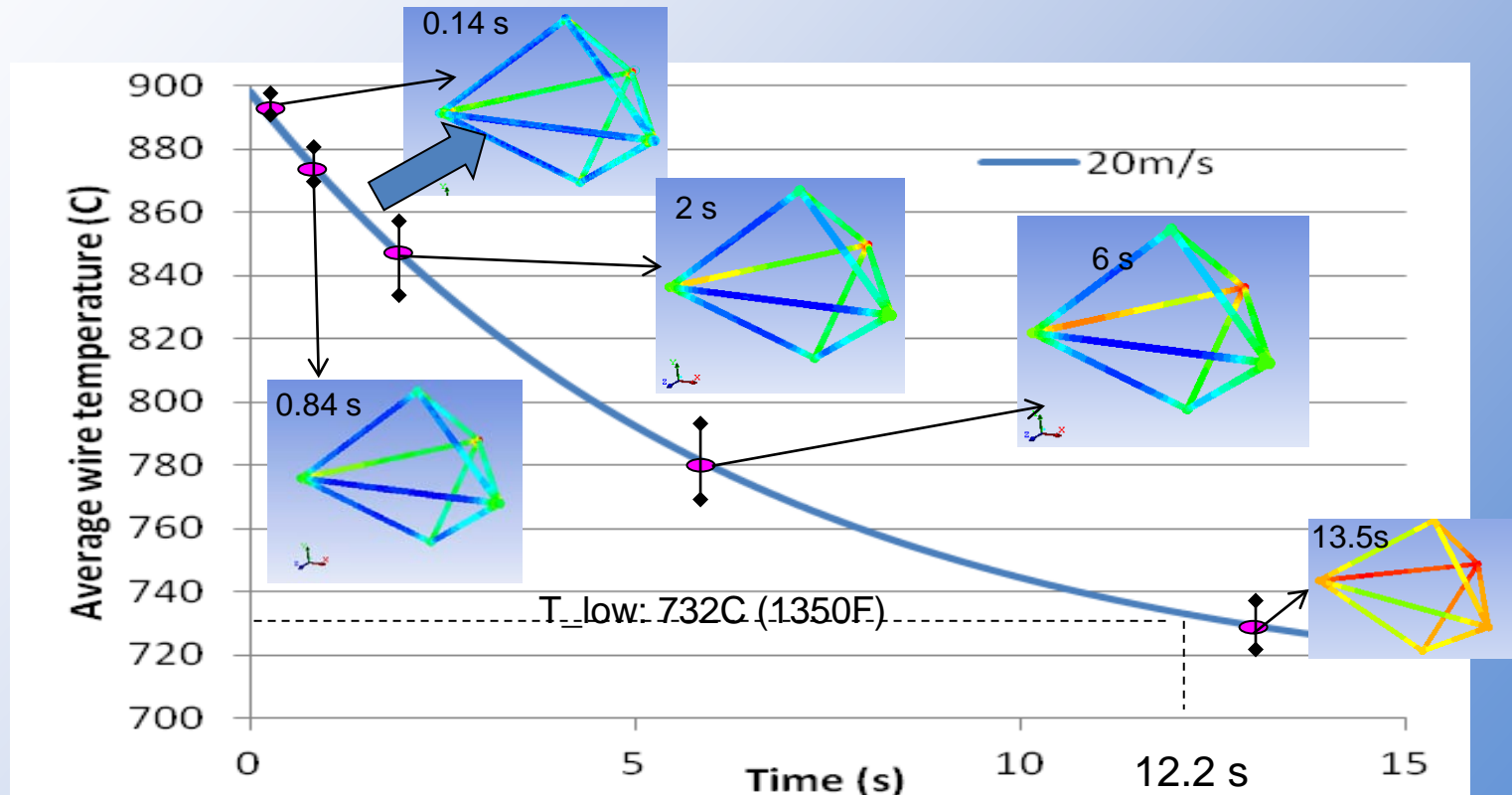
- Six members being electrically heated at 899 °C (1650°F) while being air cooled
- Three members being air cooled to 732°C (1350°F)



Air Cooling-Deactivation Mode

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To cool to ambient temperature after electrical power turn off

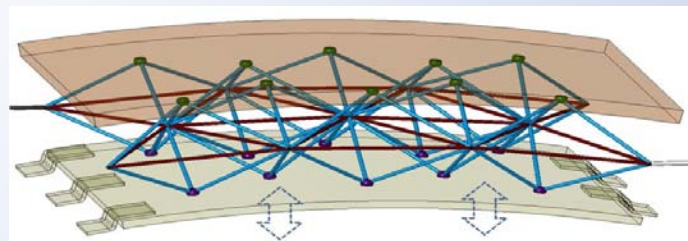
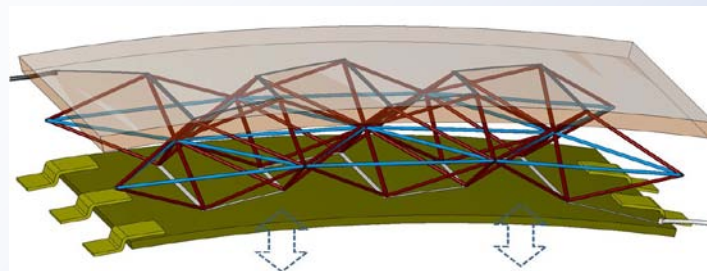


Member temperature change during cool-down with air velocity of 20 m/s



System Design Case

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Design Parameters

20 truss cells per shroud	structurally in parallel
	electrically in series
	two actuation modes
Truss cell material	Inconel 718
Therm. expansion coef.	$8.5e-6/^\circ\text{F}$
Elastic modulus	24 Mpsi
Cell dimensions	$Lb=1", d=0.059"$
Volume density	$\rho=0.11$
Design angle ω	35°

	Clearance modulation , in	Max. Deflection @ 2200, lbf	No of actuator s per shroud	No. of shroud segments	Shroud surface area, in ²	Headroom between case and shroud, in	Air temp. between case and shroud ° F	Deactivation time, s	Power to maintain activated , w
Nominal requirement*	0.05~0.1	N/A	1	20	12	2	1300	N/A	N/A
Tetrahedron truss cell	0.035	0.005	28	20	12	1.5	1650	13	1344

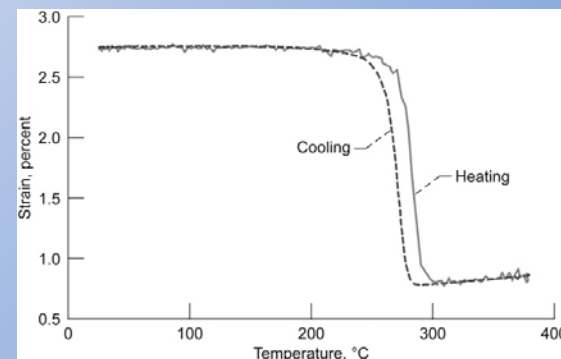
*DeCastro, 2005



Perspective on Materials

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- Baseline materials: High temperature alloys
 - Marginal CTE for large tip clearance modulation
 - Use of material phase transformation induced strain: 10x in stroke
- Commercially available Shape Memory Alloy (Nitinol SMA): 2~4% recovery and $A_f < 100^\circ\text{C}$
 - Applicable to Fan clearance modulation
- High temperature SMA in development
 - Ni30Pt20Ti50 by NASA GRC,
 - Recovery $> 2\%$ and $A_f > 250^\circ\text{C}$
 - High TRL and in useful form (NASA)
 - Applicable to HPC clearance modulation
- Ru-50 Nb and RuTa based high temperature SMA :
 - Martensitic transformation temperature $> 800^\circ\text{C}$
 - In early stage development
 - Potentially applicable to HTP clearance modulation



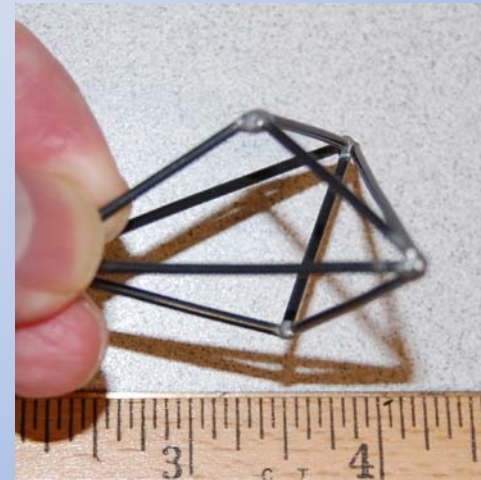
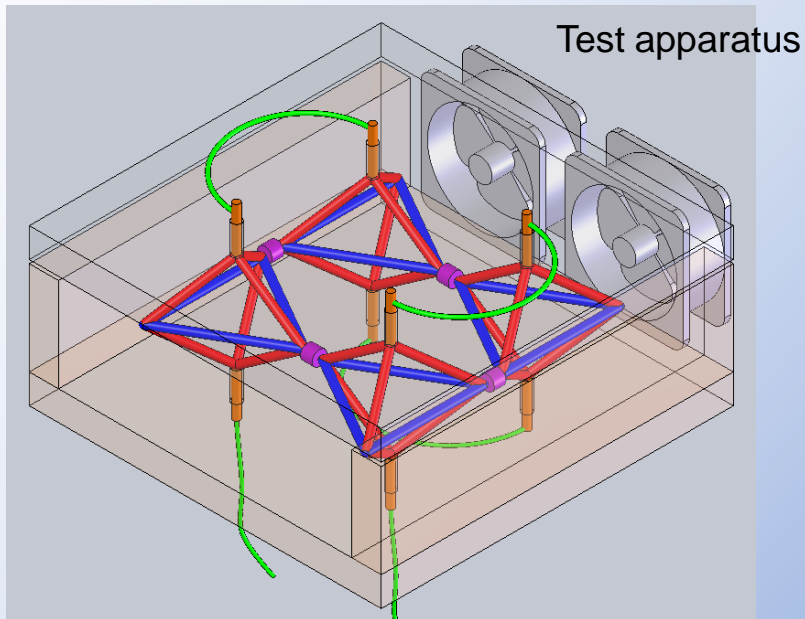
Thermo-mechanical test of Ni30Pt20Ti50 at 198 Mpa, Courtesy of NASA, M. Nathal, etc 2013



Proof of Concept Experiment

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In progress

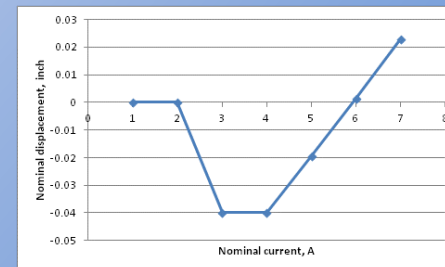


Nitinol Tetrahedron Actuator

- Thermal expansion : $6.1 \times 10^{-6} / ^\circ\text{F}$
- Electrical resistivity : $39 \text{ m}\Omega\text{-in}$

Qualitatively Evaluation of

- Displacement output
 - Linear and binary thermal expansion
- Response time in cooling
- Structural stiffness



Anticipated results



Summary

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- Active truss tip clearance modulation by thermal expansion is conceptually viable
 - kinematically, structurally and thermally
- Fast response is analytically verified to be within tens of seconds at HPT environment
- Modulation by material linear thermal expansion is adequate for small and mi-size engines
- Experimental validation of tetrahedron truss actuation in progress
- Challenges identified in materials
 - High induced strain for large transport engine
 - High temperature to enable HPT
 - High resistivity to ease direct electric heating

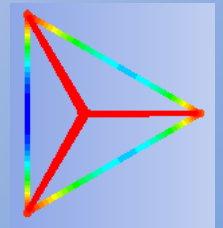


Next Steps

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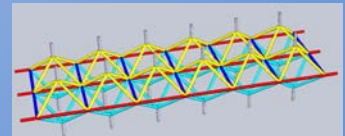
•LEARN Phase I

- Enhance modeling fidelity of single cell-truss actuation
 - Structural FEM model close loop with air cooling models
 - Air cooling models close loop with electric heating
- Experimental validation of Tetrahedron Actuation in room temperature.



•LEARN Phase II

- Expanding structural and air cooling models to large scale repetitive Active Truss Matrix structure
- Notional design and analysis of tip modulation on a notional engine
- Electric heating and control of truss modulation
- High temperature shape memory alloy (HTSMA)





Distribution/Dissemination

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In 2012, NARI awarded ARMD LEARN Fund grants to make deliberate investments in early-stage and potentially revolutionary aviation concepts and technologies that are aligned with NASA's mission. These grants went to teams external to NASA. The objectives of this three-day seminar are to increase awareness of LEARN activities within NASA projects, to provide technical feedback to LEARN principal investigators, and educate/inform the public. This will help facilitate transfer of LEARN-developed technologies within NASA and disseminate LEARN findings to the external aeronautics community, including academia, industry, and the general public.

Distribution and dissemination are unlimited