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Centrifugally Powered Pneumatic Deicing for Helicopter Rotor Blades

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NASA Aeronautics Research Mission Directorate (ARMD)

FY12 LEARN Phase I Technical Seminar

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POC: Eric Kreeger, Icing Branch/RTI, NASA Glenn



Agenda



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- Background and Motivation
- Objectives
- Prototype Design/Fabrication
- Aerodynamic Testing
- Rotor Ice Testing Results
- Erosion Testing
- Conclusions





Motivation

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Helicopter icing is introduced by both its mission requirements and operation environments:

- Urgent transportation
- Search and rescue
- Low altitude
- Low temperature
- High humidity, icing cloud possible



- ▶ **Ultimate goal of helicopter icing research: All weather aircraft**
- ▶ **Need for fundamental research to:**
 - ▶ **Improve and validate ice accretion tools**
 - ▶ **Develop and evaluate ice protection systems and protective surfaces**
 - ▶ **Develop facilities and testing procedures**



Motivation – Electrothermal Deicing

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- Only system qualified by the FAA and the DoD
- Heavy system (4 Blades 12,000 lbs Model: >160 lbs.)
- Does not allow for continuous application due to high power consumption (4 Blades, 12,000 lbs Vehicle: >20 KW, ~25 W/in²)
- Allows ice accretion up to 0.3 in (10% Torque Increase)
- Melted ice may flow aft and refreeze further
- Difficult to integrate with polymer erosion-resistant materials



*ARMY HISS Icing Certification Testing
Ice Protection System (S-92™)*

A low-power, non-thermal IPS is desired to have an impact on all-weather capabilities:

- **Compatibility with smaller vehicles**
- **Compatibility with polymer leading edges**



Background



- Pneumatic de-icing boots → used on fixed-wing aircraft for decades
- In the 80's, NASA and Goodrich attempted to develop **rotorcraft** de-icing boots
- Boots were successful in de-icing rotor blades, several problems were identified:
 - 1) Complicated pneumatic slip-ring transferred engine bleed air out to rotating frame
 - 2) Erosion of polymer boots
 - 3) Altered airfoil shape led to rotor performance degradation
- These problems were technology development barriers

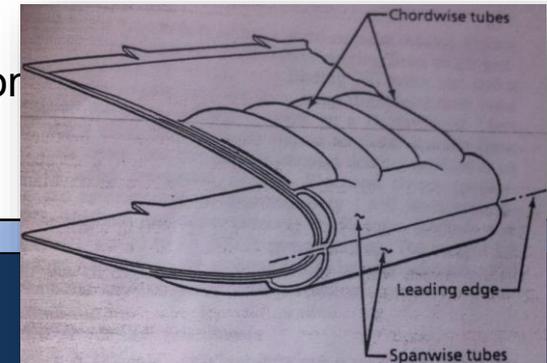


Fig. 1. Photo JUH-1 test helicopter

The Innovation:

- Avoid pneumatic slip rings:
CENTRIFUGAL PUMPING
- Avoid pneumatic diaphragm exposure:
Ti-Al-N Erosion resistant coating
- Avoid rotor performance degradation:
CONTROLLED DEFLECTION ZONES



Centrifugally Powered Pneumatic De-Icing Concept



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Goal: Surface De-Icing Treatment can be Retrofitted to Existing Blades

- No Pneumatic Slip Ring
- Insignificant Electrical Power Use
- Insignificant Added Blade Weight

$$\frac{dp}{dr} = \rho(r)r\Omega^2$$

p = Pressure, ρ = Density, r = Radius, Ω = Rotor Speed

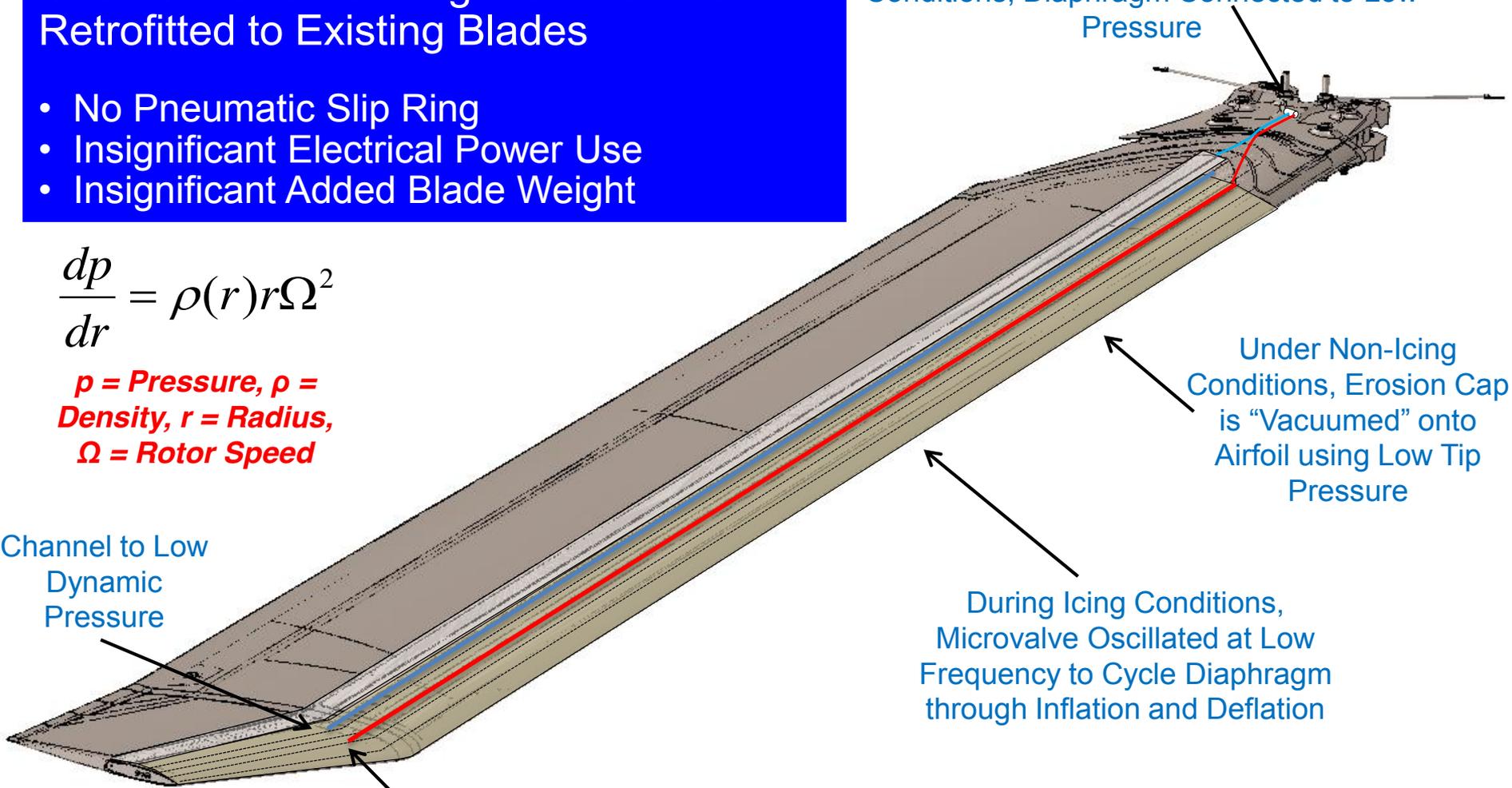
3-Way Microvalve Off under Non-icing Conditions, Diaphragm Connected to Low Pressure

Under Non-Icing Conditions, Erosion Cap is "Vacuumed" onto Airfoil using Low Tip Pressure

During Icing Conditions, Microvalve Oscillated at Low Frequency to Cycle Diaphragm through Inflation and Deflation

Channel to Low Dynamic Pressure

Channel Sealed at Tip





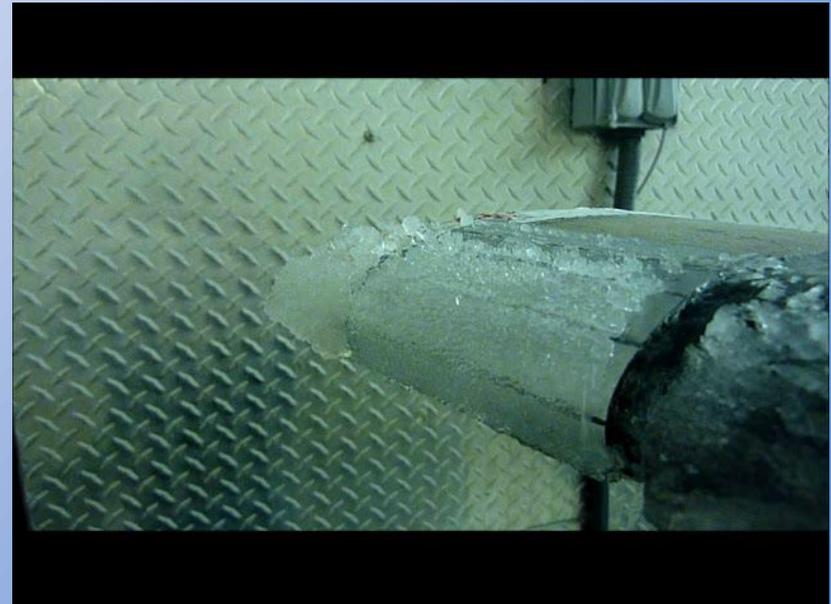
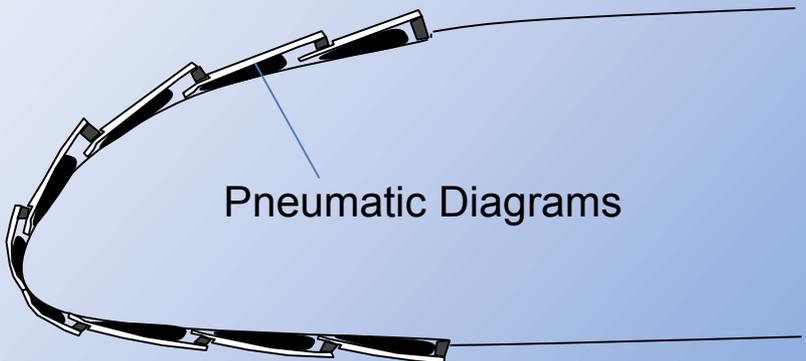
Proof-of-concept: Pneumatic Deicing



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- Initial designs considered allowed for local deformation of individual 0.02" thick Ti strips
- Goal: minimal impact on existing blade design (surface treatment)
- Power Consumption: **< 1 W of power with no insignificant additional blade weight**

Design 1





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Objectives



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- 1) To conduct rotor icing experimental testing of a centrifugally powered pneumatic de-icing prototype for helicopter rotor blades
- 2) To confirm the system effectiveness:
 - Low-power consumption
 - Robustness under centrifugal loads (CF)
 - Reduced aerodynamic penalty
 - Erosion resistance

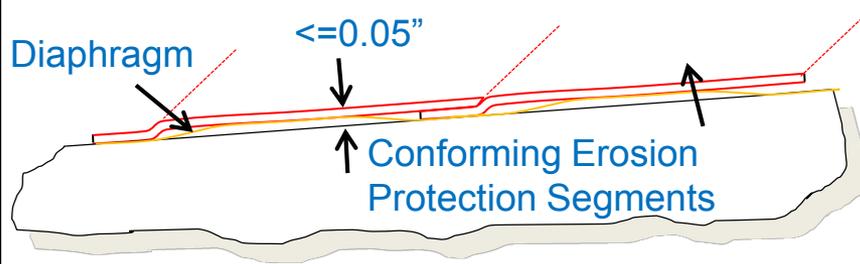
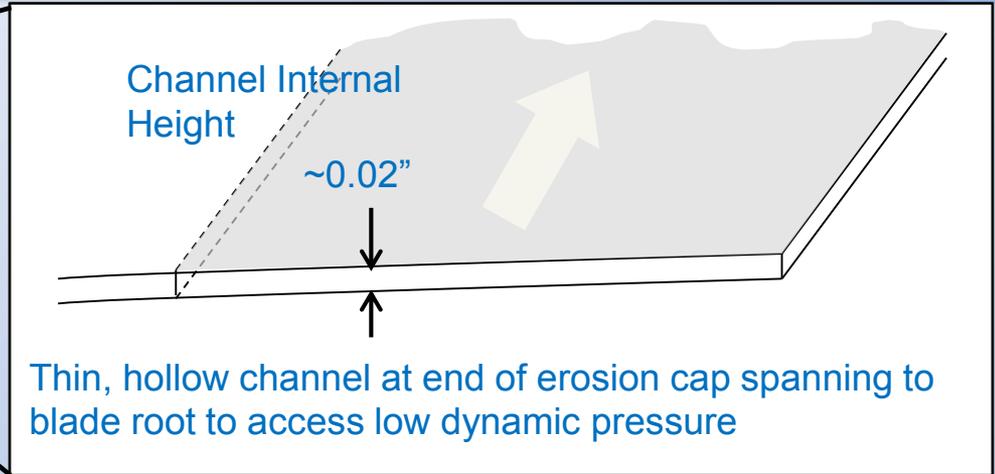


Pneumatic De-Icing Design: Prototype I

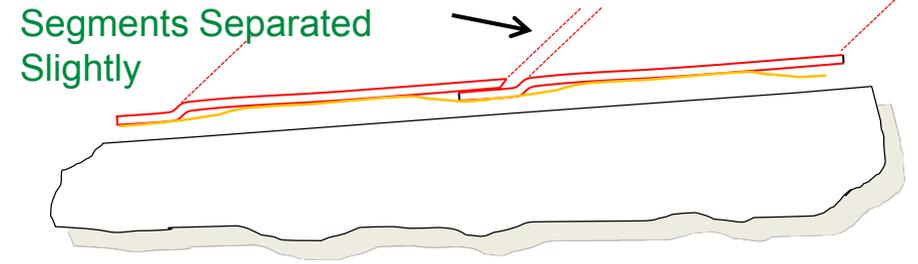


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Blade Tip



- Power off condition. Volume under diaphragm connected to low dynamic pressure
- Erosion segments conform to desired airfoil shape
- Leading edge maintains rigidity



- Microvalve activated at root
- Volume under diaphragm allowed to inflate slightly under CF
- Segments pulled apart slightly, cracking ice
- Vectran bonded to airfoil at cap edges and periodically around entire leading edge

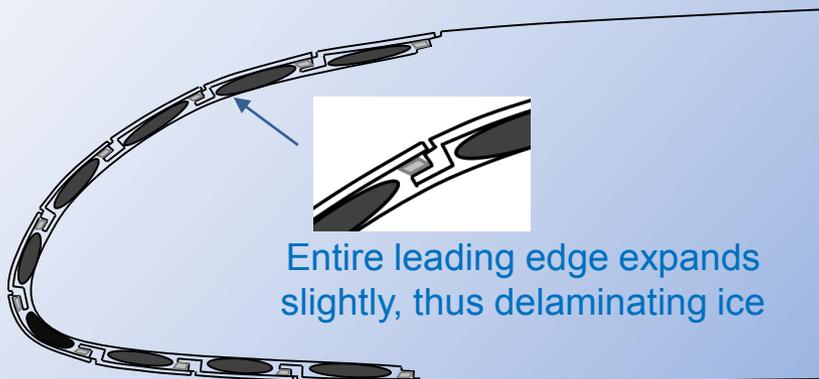
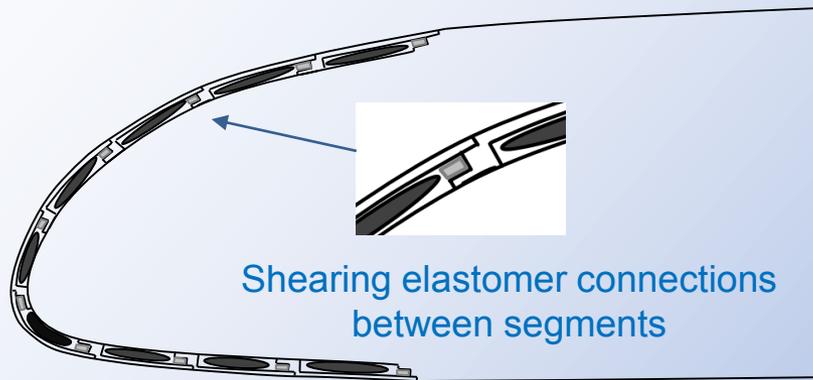


Pneumatic De-Icing Fabrication: Prototype I

PENNSYLVANIA STATE UNIVERSITY



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Electrical Discharge Machined Wire Cutting of leading edge segments



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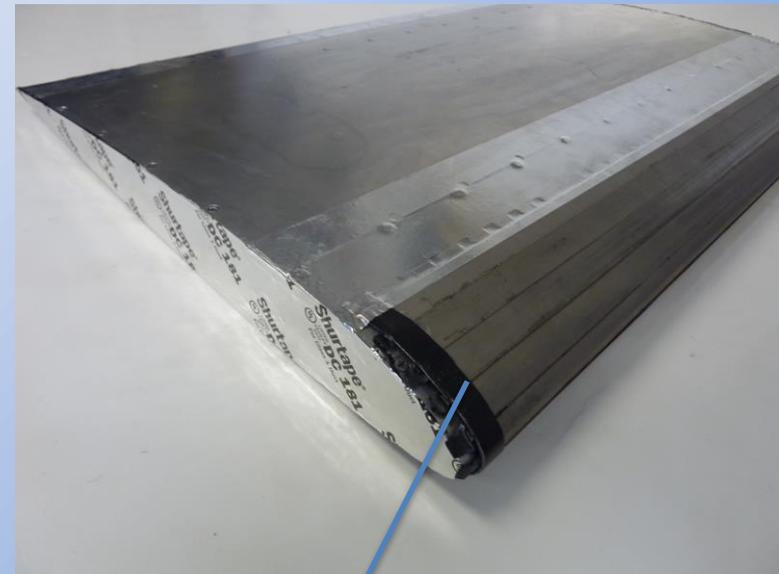
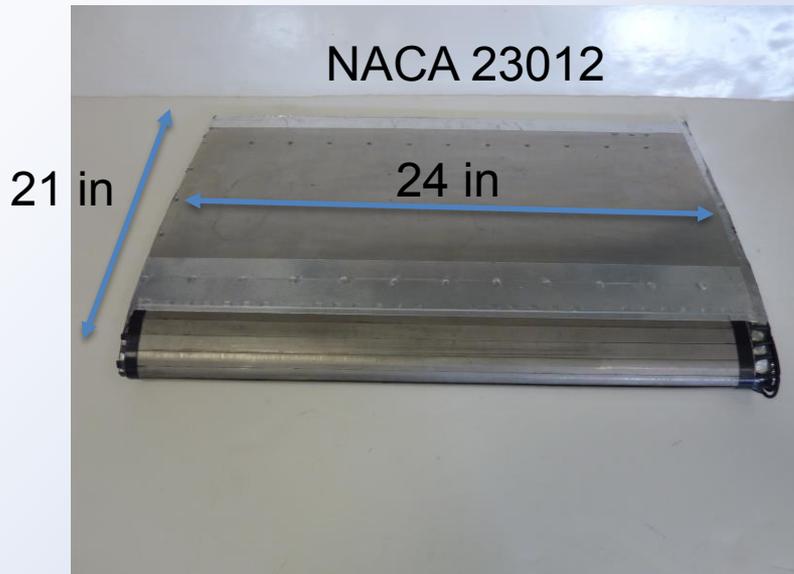




Aerodynamic Testing Prototype I



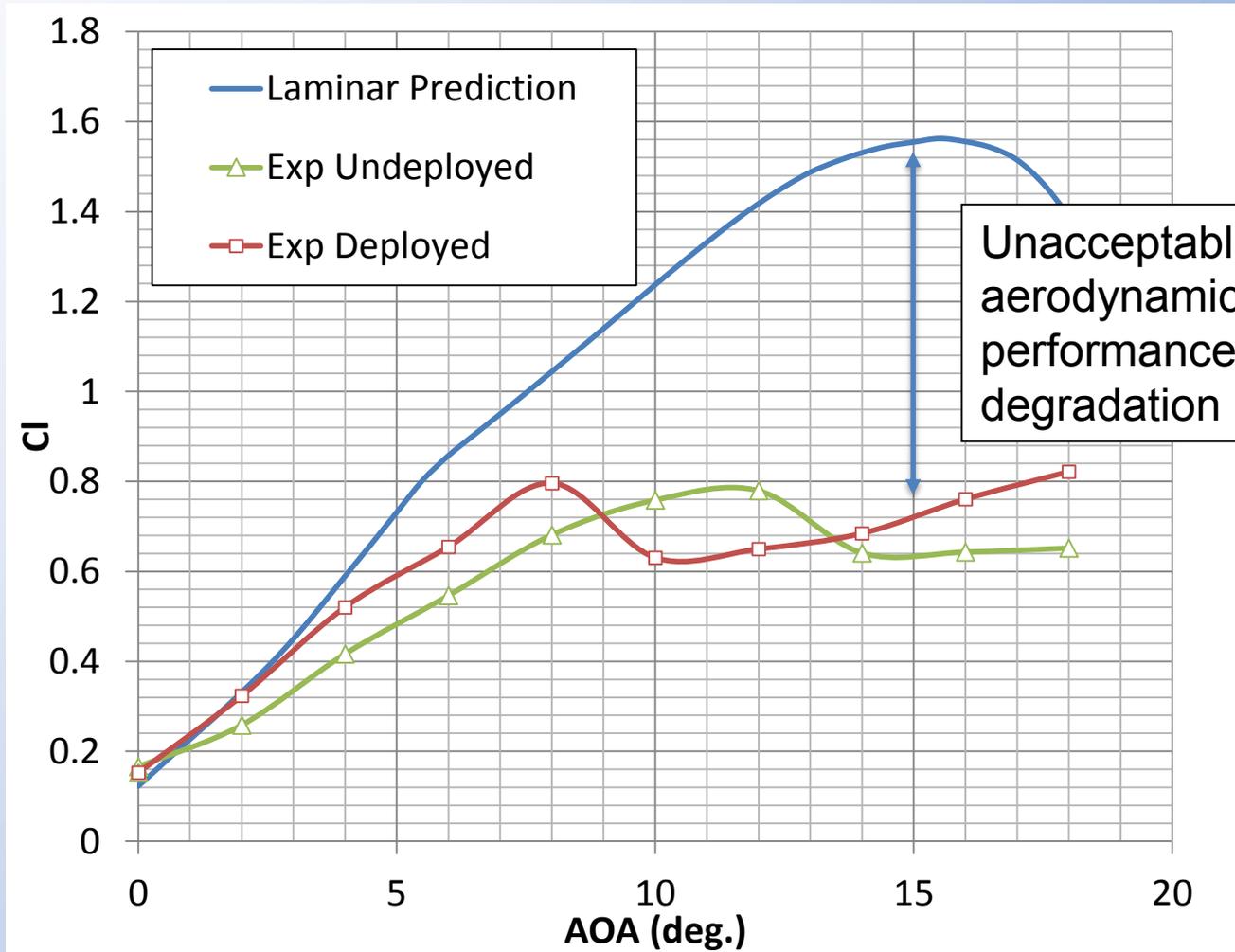
Model with deployable leading edge fabricated for wind tunnel testing



Detail of Segmented Leading Edge



Aerodynamic Testing Prototype I





Pneumatic De-Icing Concept: Prototype II

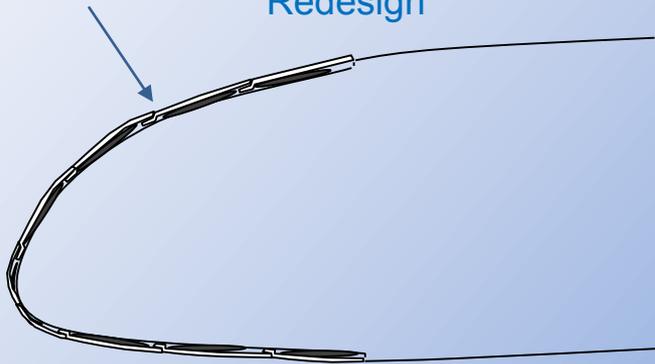


Must mitigate aerodynamic performance degradation concerns

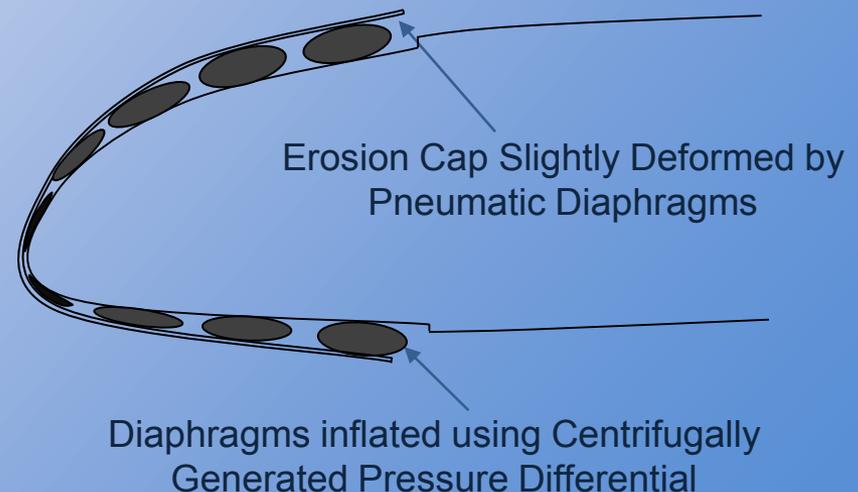
In operation, low internal blade pressure will pull the system ($\leq 0.2''$) onto the leading edge

- Conforming airfoil shape
- No major rotor aerodynamic performance degradation

Goal: Design System Thin Enough to Replace Current Erosion Caps with Little or No Blade Redesign



Exaggerated Displacement

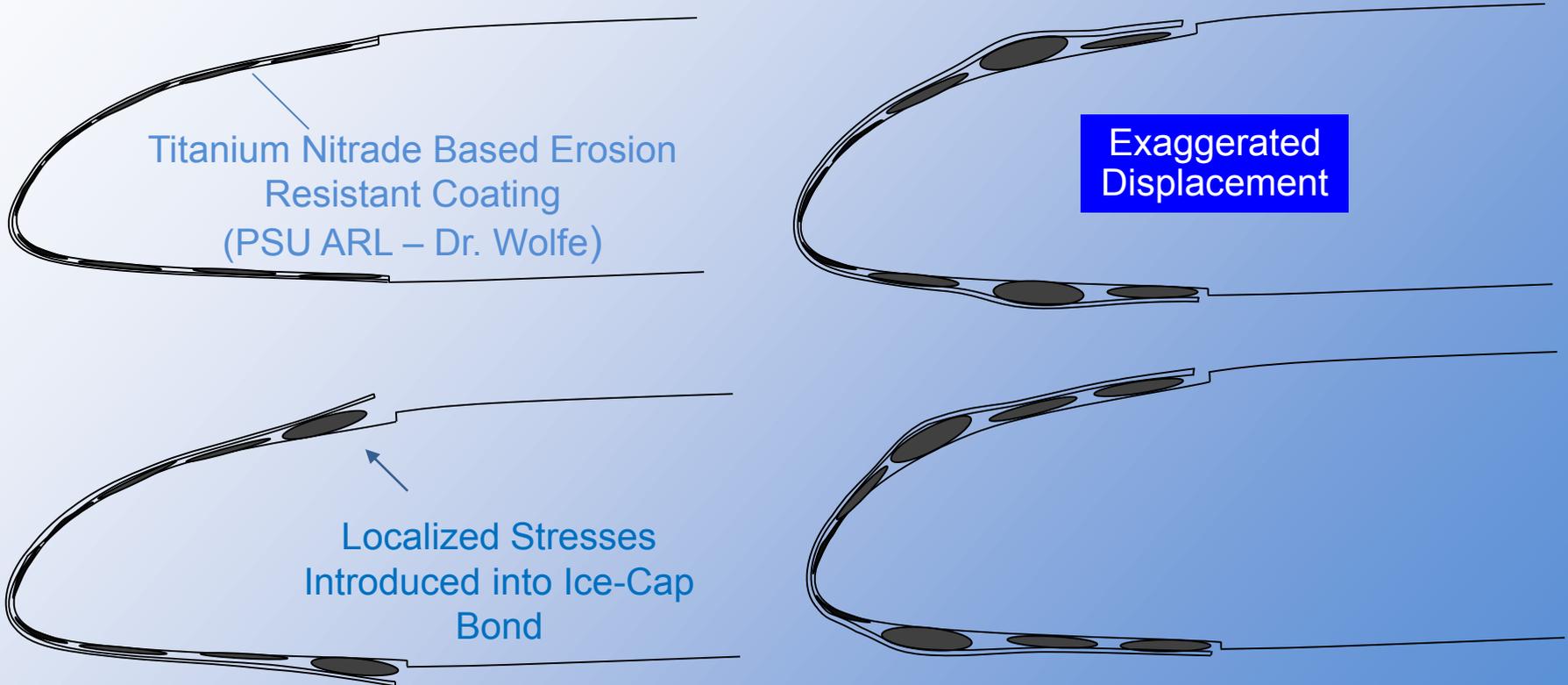




Pneumatic De-Icing Concept: Prototype II



Deflection Modes: concentrate ice interface transverse shear stresses at desired chord locations



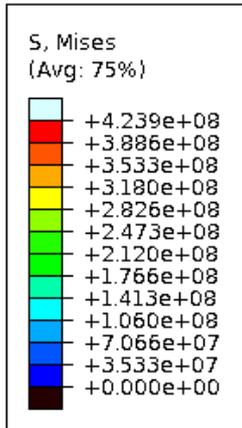


FEM Modeling

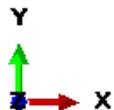
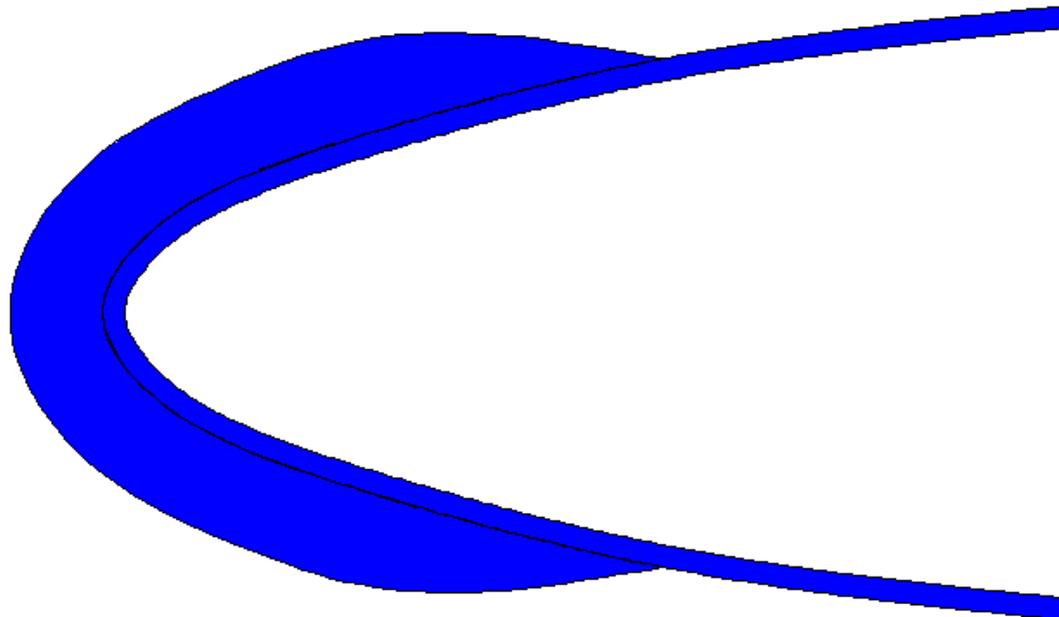


Cohesive zone method FEM

Barbero, E., "Finite Element Analysis of Composite Materials,"
2008, ISBN 9781420054330, xxv, 331



Step: Step-1 Frame: 0
Total Time: 0.000000



ODB: 2D_ice-shape.odb Abaqus/Standard 6.10-2 Mon Nov 04 13:19:17 EST 2013

Step: Step-1
Increment 0: Step Time = 0.000
Primary Var: S, Mises
Deformed Var: U Deformation Scale Factor: +1.000e+00



Aerodynamic Testing Prototype II

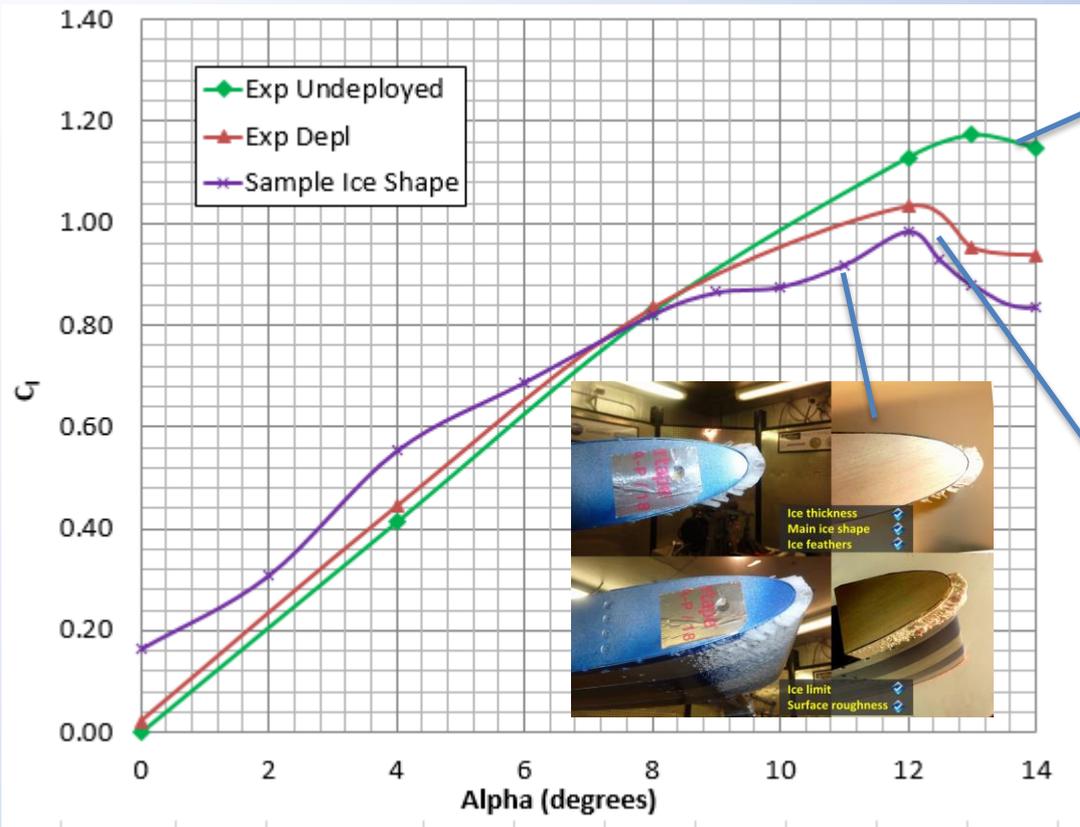


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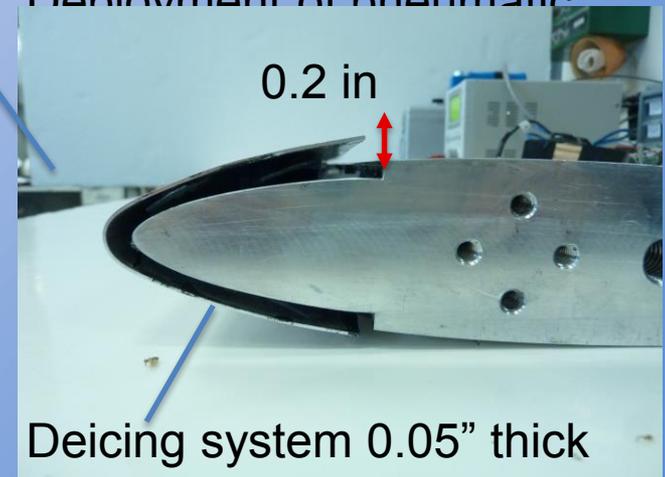


Wind Tunnel Testing Leading Edge Deployment

Cl vs Angle of Attack



Deployment of pneumatic



Deicing system 0.05" thick

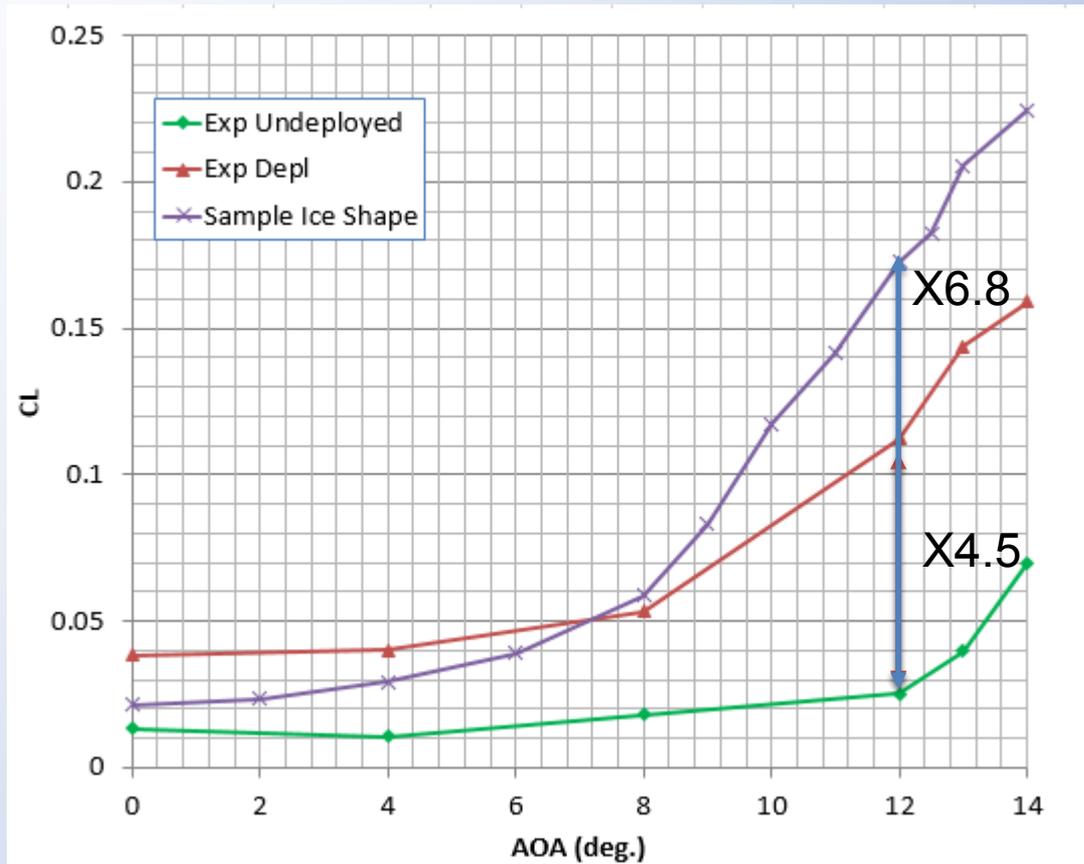


Aerodynamic Testing Prototype II: Results



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Cd vs Angle of Attack



Deployment of pneumatic deicing degrades the drag performance of the airfoil.

The performance penalty does not exceed the degradation related to ice accretion.



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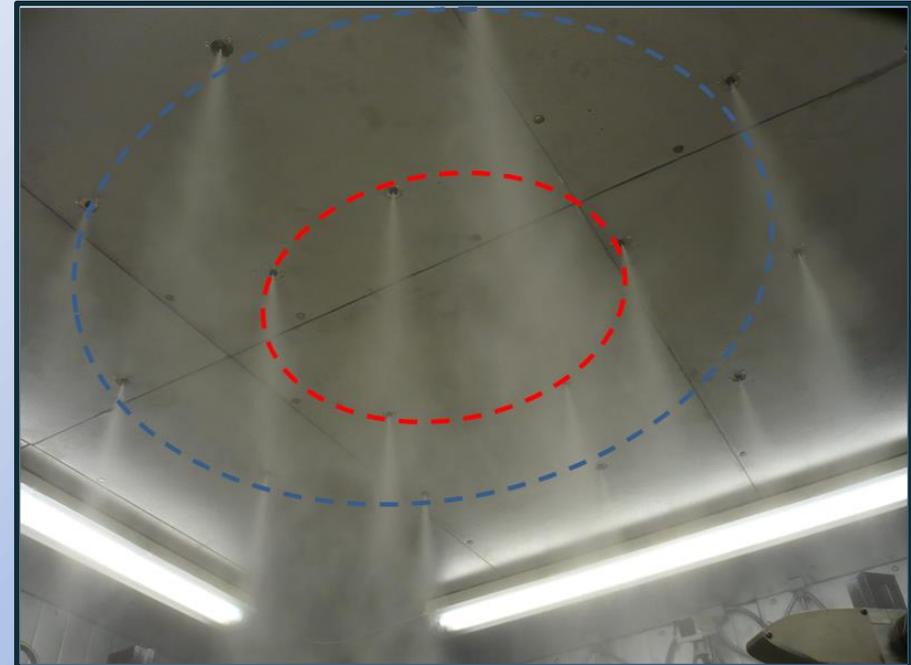


Testing Facility



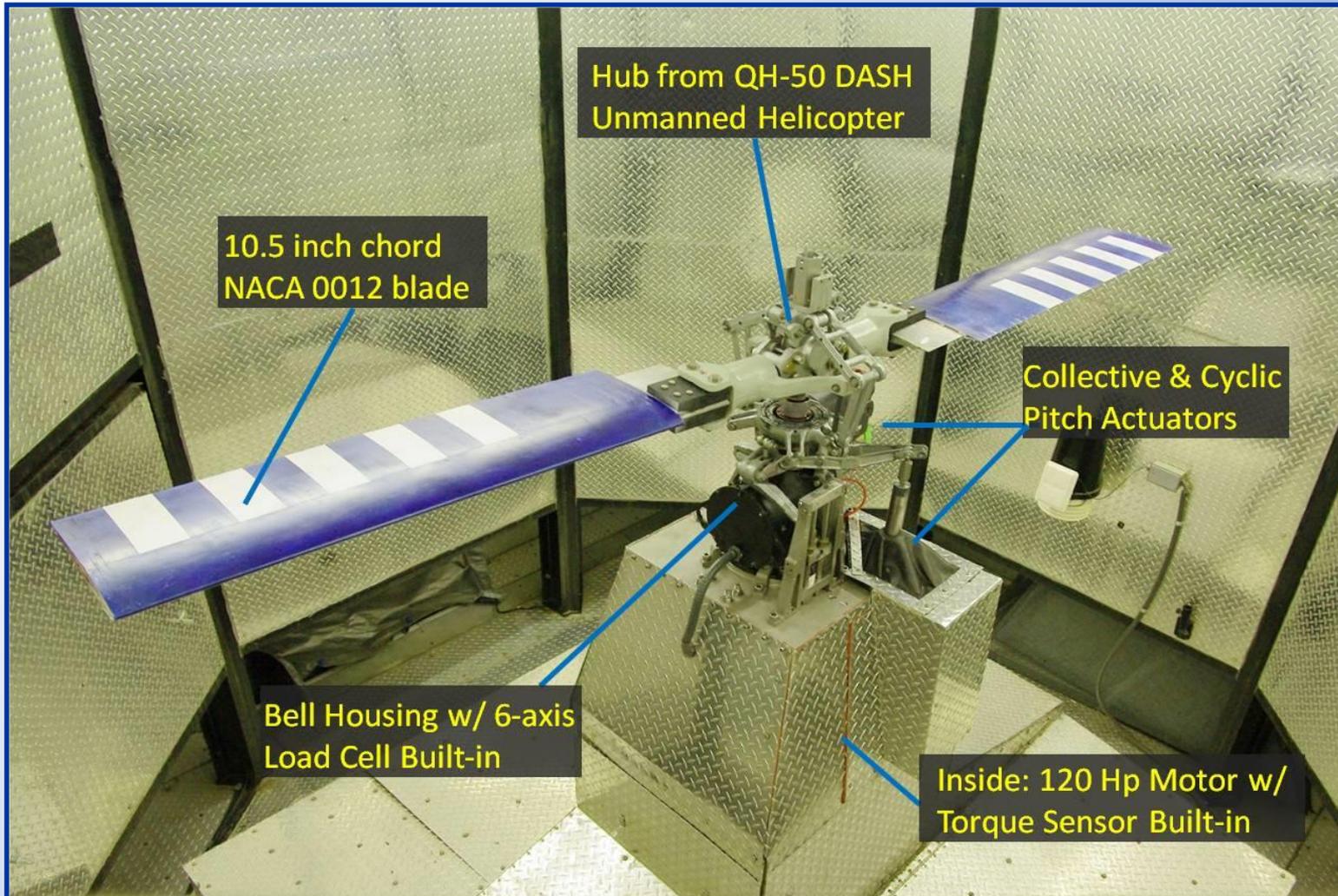
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Parameter	Range
LWC [g/m^3]	0.1 ~ 5 (increments of 0.2)
MVD [μm]	10 ~ 50
Temperature [$^{\circ}\text{C}$]	-20 ~ 0
Rotor Speed [RPM]	200 ~ 1200
Blade Diameter	3 [m] / 10 [ft]
Blade chord	12.4 ~ 81.3 [cm] / 4.9 ~ 32[in]



Icing Nozzles control LWC and MVD

- ▶ Signal and Power Transmission: 48 signal / 24 power channel slip ring
- ▶ Measurement Instrument: Shaft torque sensor / 6-axis load cell
- ▶ **Facility proven to create representative icing conditions (and ice shapes)**





AERTS Facility Video



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Rotor Icing Testing Conducted at PSU AERTS



Representative Icing Conditions and Centrifugal Loads



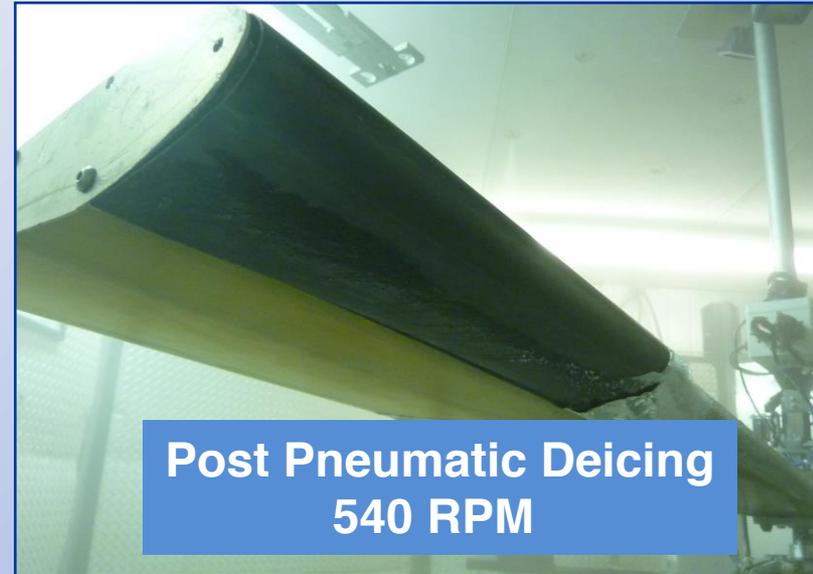
Sample Result



Pneumatic Deicing without Centrifugal Loading



Sample Result



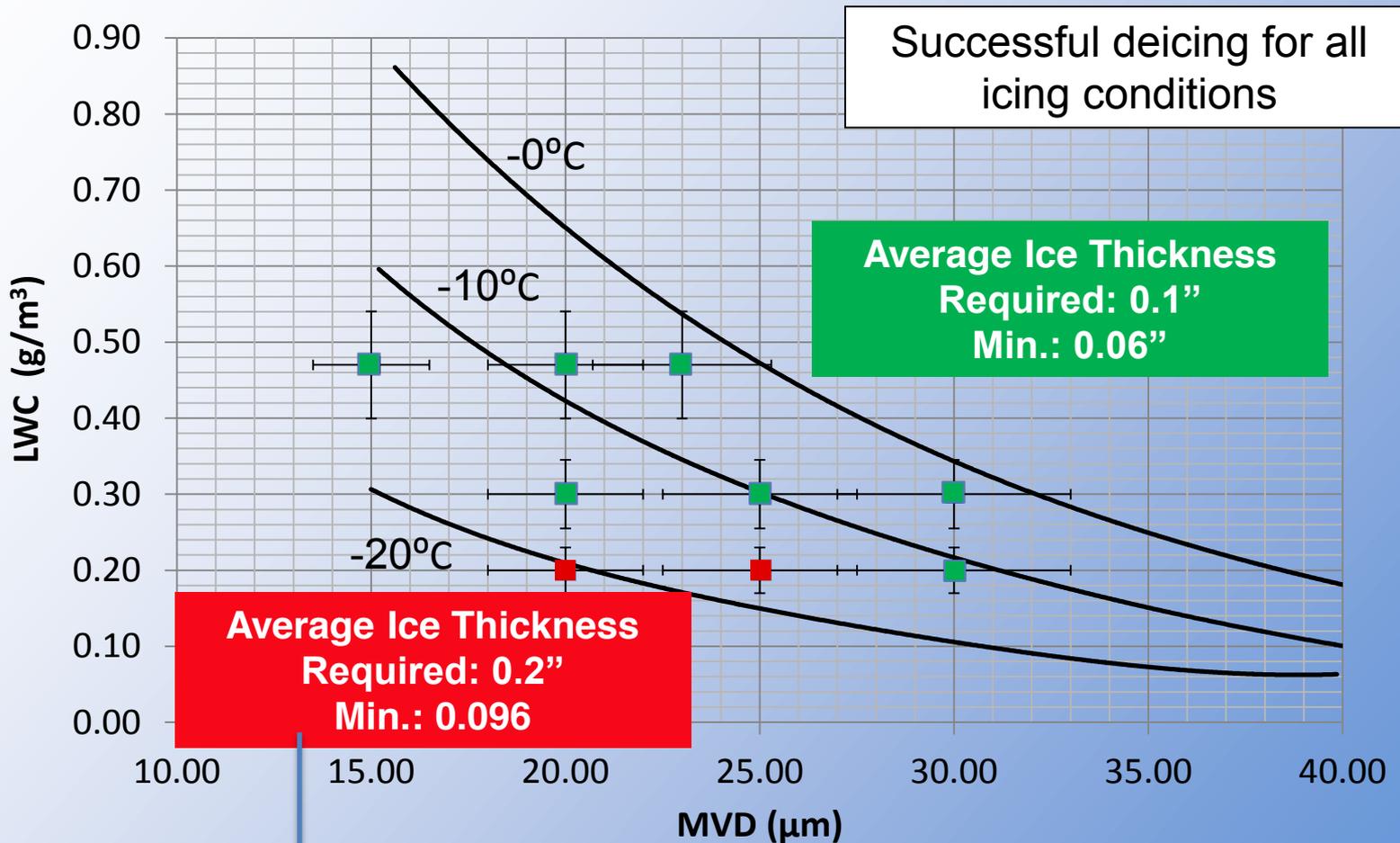
- Ice shedding was achieved at 250 RPM (20% CF) and 540 RPM (90% CF)
- Ice thickness as small as 0.06" were shed at temp. above -15 deg. C
- Air pressure used +/- 3.7 psi (representative rotor blade generation)
- Electrical power consumption: 2.9 Watts



Continuous Icing Cloud Test Results



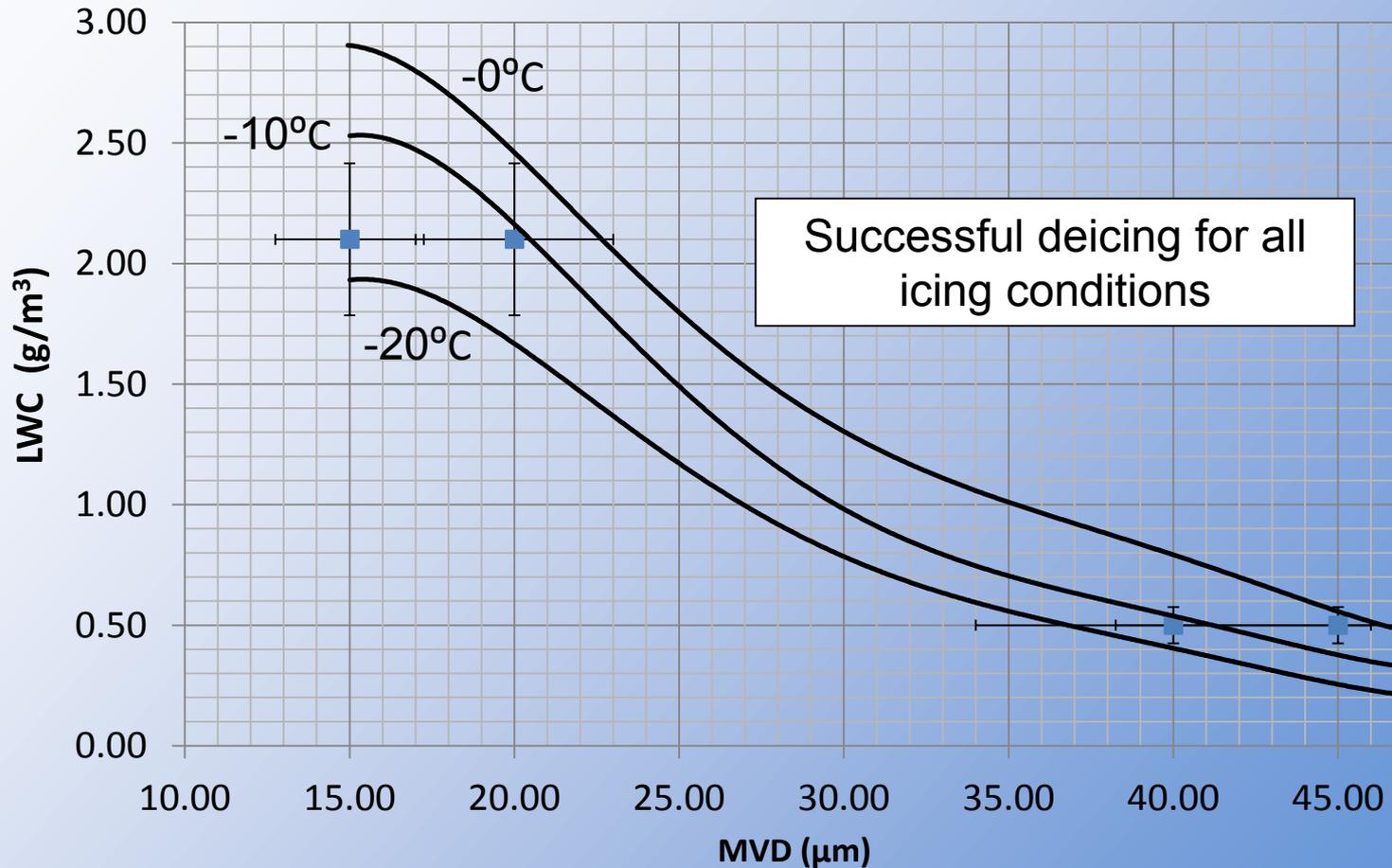
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Diaphragm material stiffens beyond pressure capabilities at Temp. < -15°



Intermittent Icing Cloud Test Results





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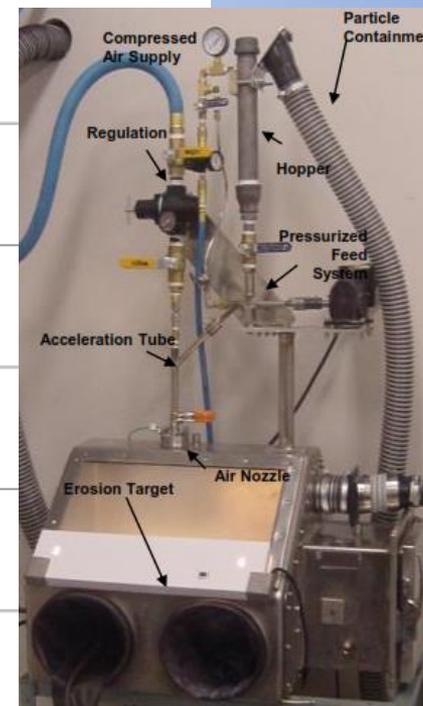
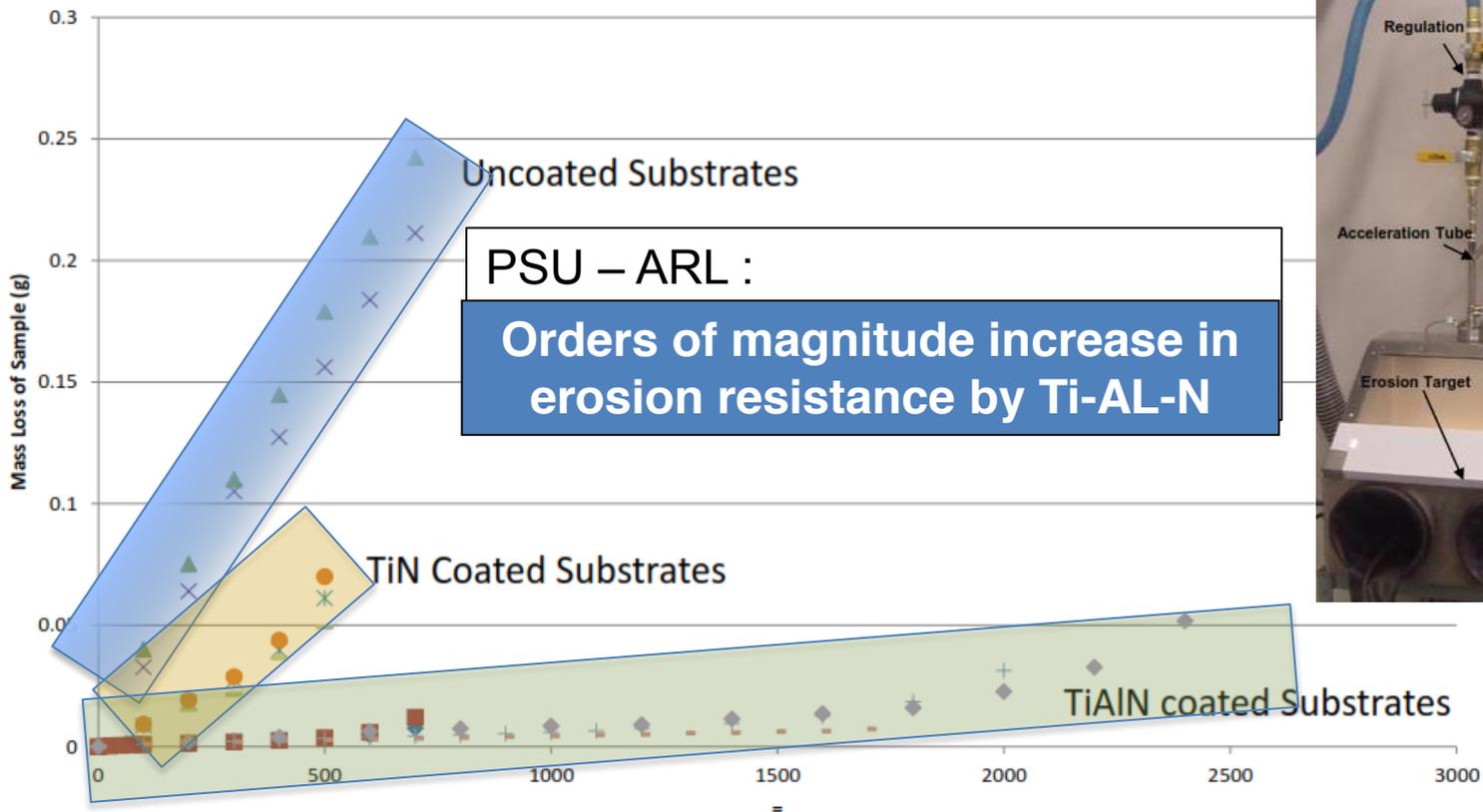


Proof-of-concept: Erosion Resistance Coating



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Erosion data, 30 degrees, 156m/s, 240 grit (50um) alumina, 1.125" wear diameter, 9" Stand-off distance, 100g/min feed



× Uncoated Ti 6-4	▲ Uncoated SS 17-PH4	× C100317-1 T40(#) TiN on Ti	— C100317-1 T40 TiN on Ti	● C100317-1 S82 TiN on SS
◆ C100304-1 S72 TiAlN on SS	■ C100304-1 T26B TiAlN on Ti	+ C100311 T36(#) TiAlN on Ti	- C100311-1 T36 TiAlN on Ti	◆ S100311-1 S77 TiAlN on Ti

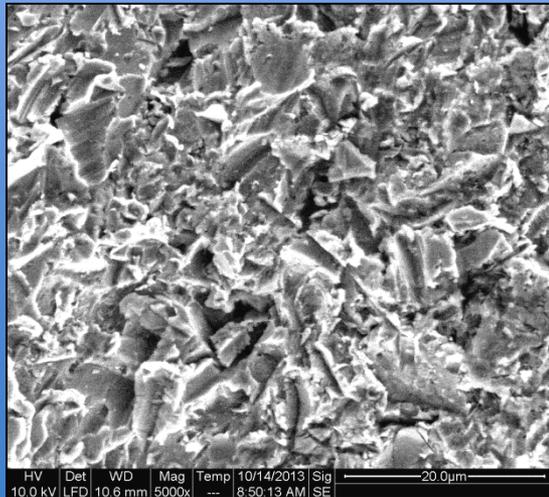
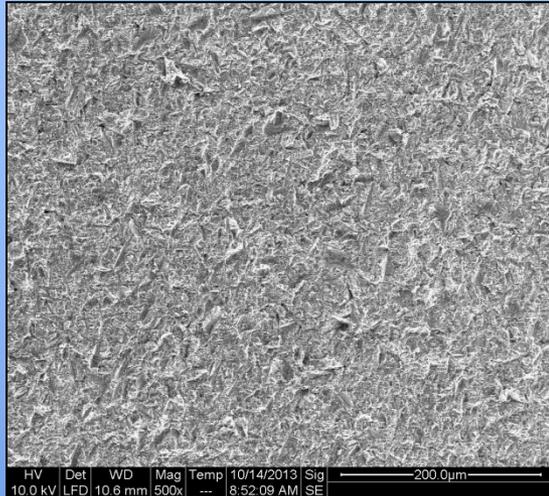


Erosion Testing Ti-AL-N Coating: SEM Surface Morphology 500 g. Exposure

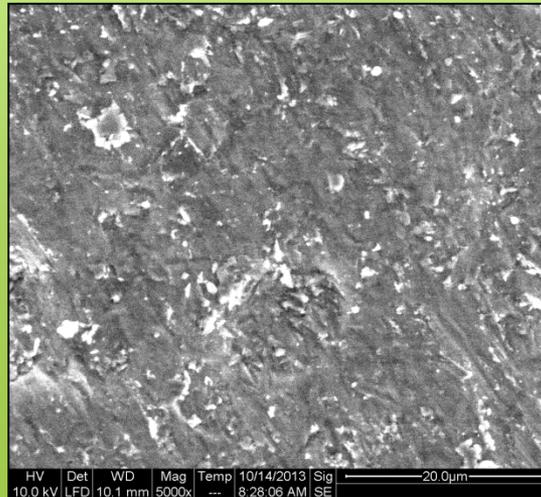
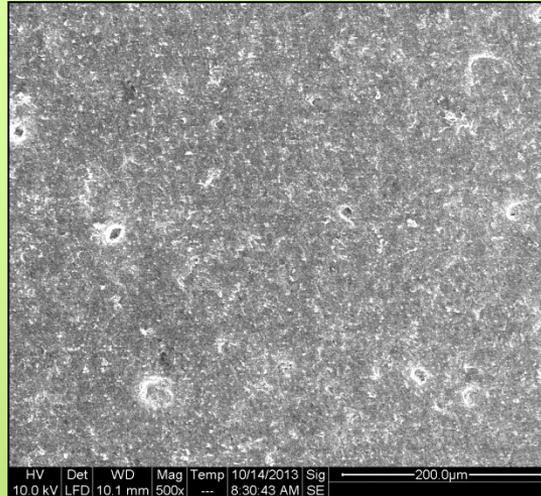


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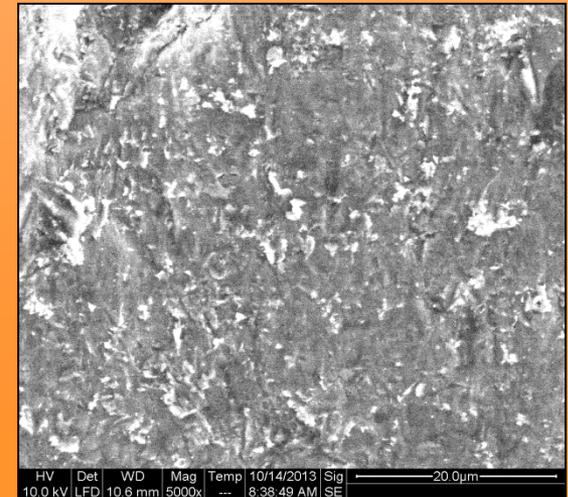
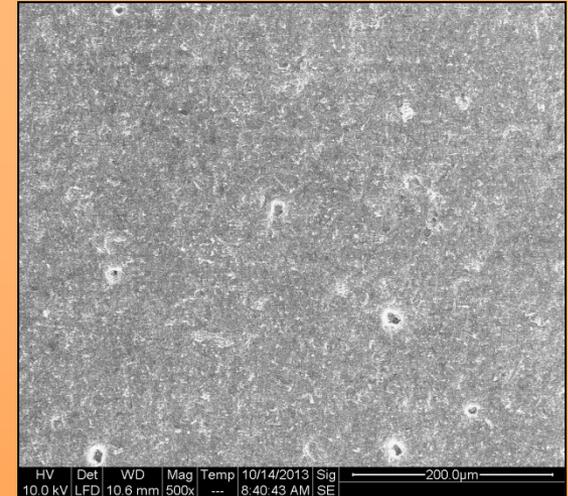
Uncoated Ti



Ti-AL-N: 100µin Thick



Ti-AL-N: 200µin Thick



30 degrees, 156m/s, 50 µm alumina, 0.5 wear diameter, 9" stand-off distance, 100g/min



Conclusions



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- Smooth leading edge configurations are critical to avoid aerodynamic performance degradation of the blade
- Aerodynamic performance degradation due to system deployment was less than the effects of the ice accretion
- The proposed pneumatic deicing configuration is able to delaminate ice accretion (Appendix C icing envelope) with input pressures as low as +/- 3.7 psi.
- Ice thickness as small as 0.06 in. were successfully removed for temperatures above -15 deg. C.
- The maximum ice thickness needed to promote ice delamination at colder temperatures could reach up to 0.2 in. (comparable to ice accretion allowed by electrothermal deicing).
- The larger ice thickness requirements are attributed to the stiffening of the prototype diaphragm used
- The system performed at 90% and 20% representative CF loads
- Ti-AL-N shows orders of magnitude improvement on sand erosion resistance compared to Ti → allows for a reduction in thickness of the Ti substrate



Goal: Full-scale proof-of-concept testing

- Design system with temperature rated diaphragms
- Access a whirl tower in cold climates
- Full-scale rotor blades to be modified to accommodate pneumatic de-icing
- Design portable cloud generators
- Design an optimized de-icing system (FEM)
- Perform full-scale rotor blade pneumatic deicing
- Rock and small ballistic Impact testing



Distribution/Dissemination



- Soltis, J., Palacios, J., Wolfe, D., Eden, T., “Evaluation of Ice Adhesion Strength on Erosion Resistant Materials,” AIAA-2013-1509, 54th AIAA/ASME/ASCE/AHS/ASC Structures, Structural Dynamics, and Materials Conference, 2013, Boston, Massachusetts, April 8 – 11, 2013.
- Abstract submitted to the American Helicopter Society 70th Forum.
- Briefing given to Bell on April 2013
- Briefing given to Sikorsky on June 2013
- Briefing given to Boeing on July 2013
- Rotor Icing and Protection Demonstration given to Boeing on September 2013
- Rotor Icing and Protection Demonstration to be given to NASA and GE on Nov – Dec 2013 (POSTPONED)



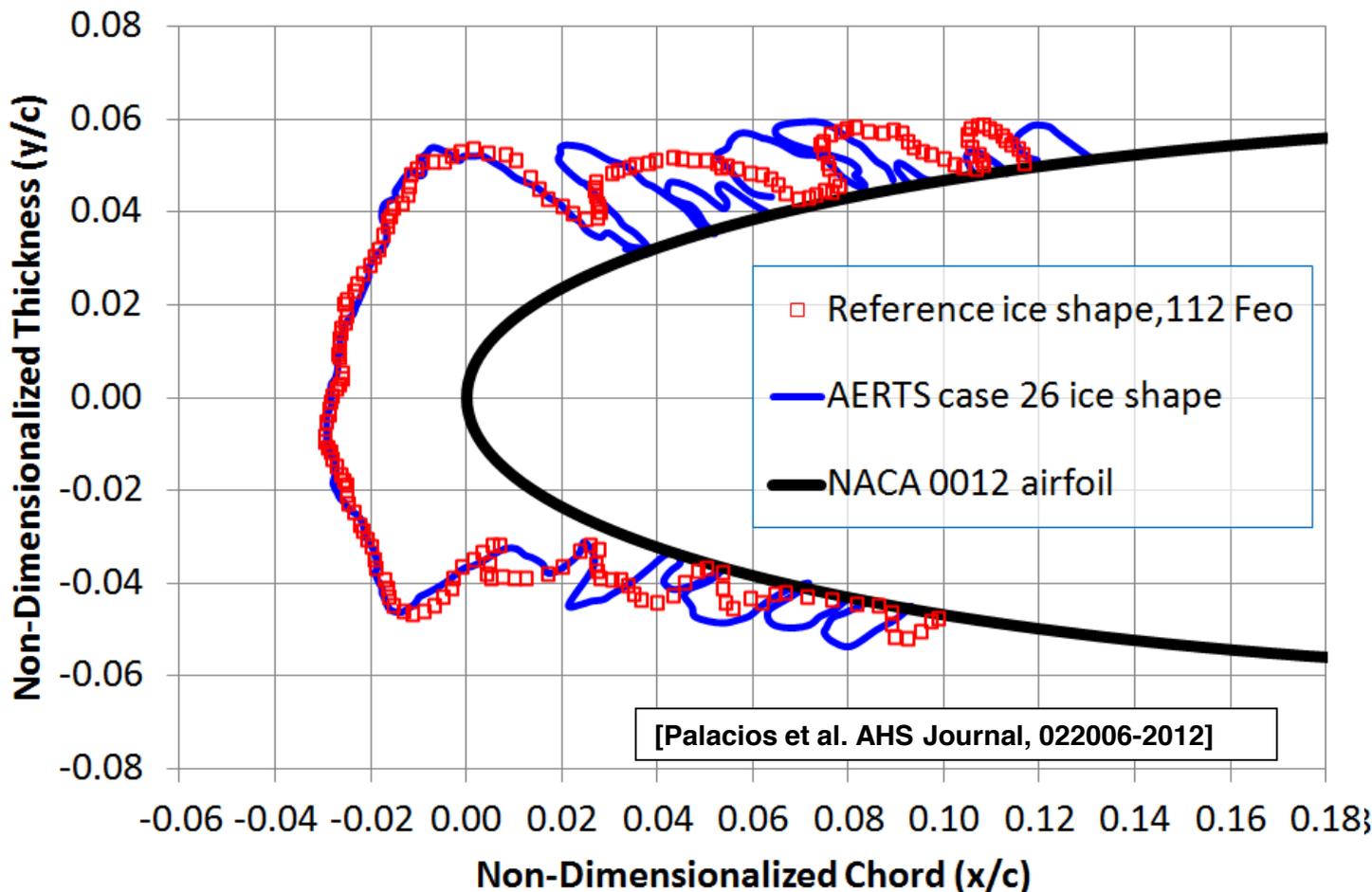
Questions?



Ice Shape Correlation: Facility Validation



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Case	Chord	MVD	LWC	Temp.	V	Time	AOA	RPM
26, 112	10.5"	27	0.96	-8.2	56.9	4.2'	0	417.21